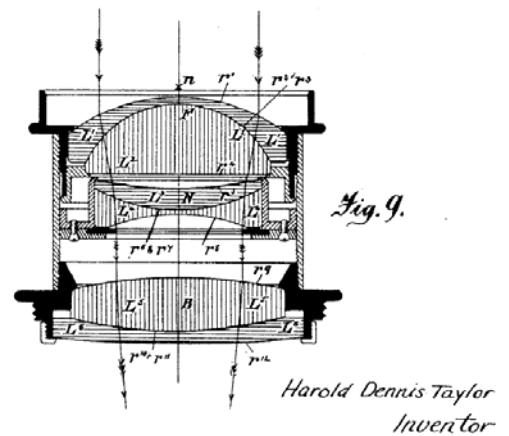


# Design of a Cooke Triplet

May 6, 2009

Wonjoon Choi  
Ryan Cooper  
Qunya Ong  
Matthew Smith



# Basics of a Cooke Triplet

- Composition: a negative lens with low V-value (flint) between two lens with high V-values (crowns)
- Feature: the smallest number of elements that can correct all 7 Seidel aberrations:
  - *Monochromatic:* spherical aberration, coma, astigmatism, field curvature, distortion.
  - *Chromatic:* axial chromatic aberration and lateral chromatic aberration.
- Design Principles:
  - Choice of lens powers such that their sum  $\sim 0$
  - Use of spaced positive and negative lenses
  - Use of approximate front-to-back symmetry

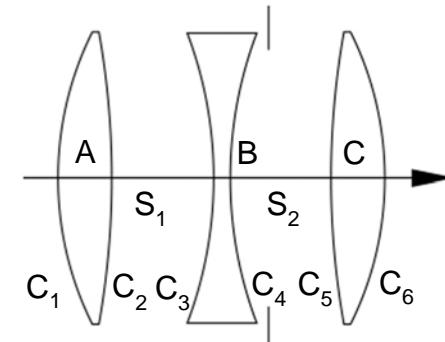
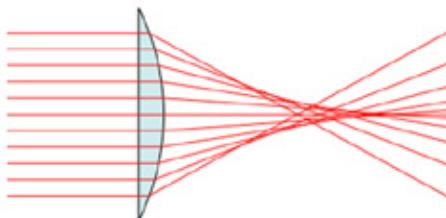
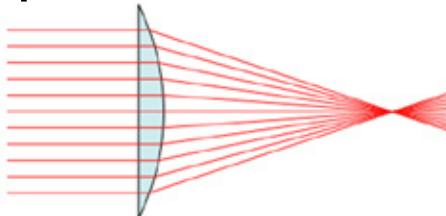


Image from [Wikimedia Commons](#).

# Monochromatic Seidel Aberrations

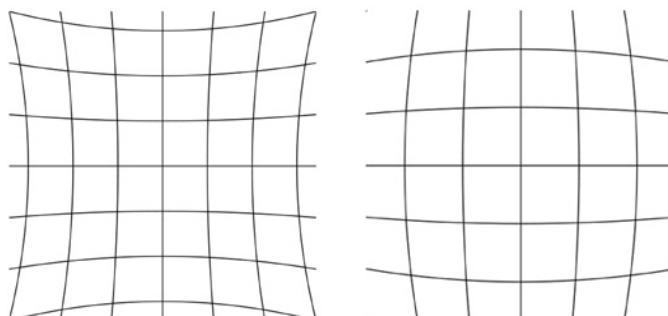
- Spherical aberration:



- Coma:

<http://commons.wikimedia.org/wiki/File:Lens-coma.svg>

- Distortion:



- Astigmatism:

<http://commons.wikimedia.org/wiki/File:Astigmatism.svg>

- Field curvature:

Images removed due to copyright restrictions. Please see Fig. 5.2, 5.4, 5.7, 5.8, and 5.9 in Smith, W. *Modern Optical Engineering*.

# Design Objective

- Design a Cooke Triplet with minimal Seidel aberrations using Zemax to vary the available degrees of freedom:

- ✓ 6 curvatures
- ✓ 3 lens thicknesses
- ✓ 2 air spaces
- ✓ 3 glass choices

**Total: 14 Variables**

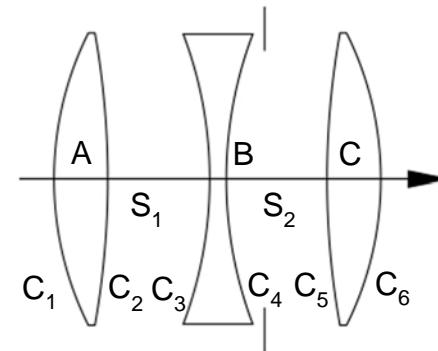
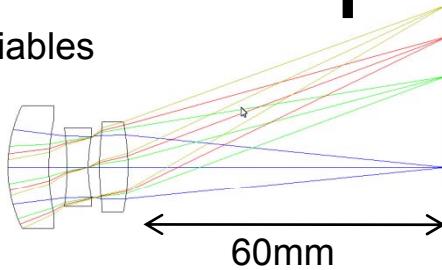


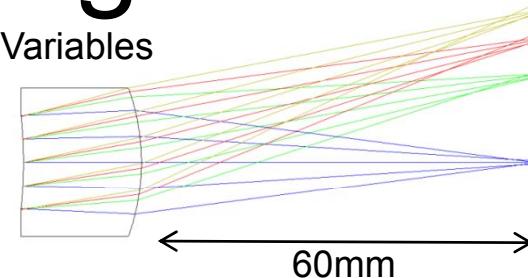
Image from [Wikimedia Commons](#).

# Cooke Triplet vs. Single Lens

14 Variables



4 Variables



$$\lambda=0.486 \mu\text{m}$$

$$0.588 \mu\text{m}$$

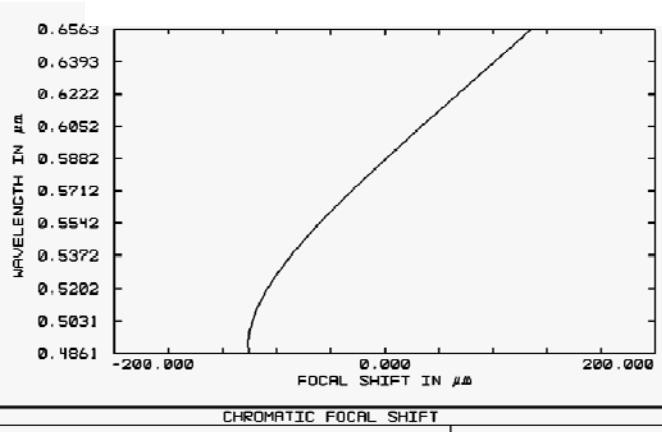
$$0.656 \mu\text{m}$$

$$0^\circ$$

$$13.57^\circ$$

$$19.10^\circ$$

$$23.40^\circ$$



Spot  
diagrams

$$\lambda=0.486 \mu\text{m}$$

$$0.588 \mu\text{m}$$

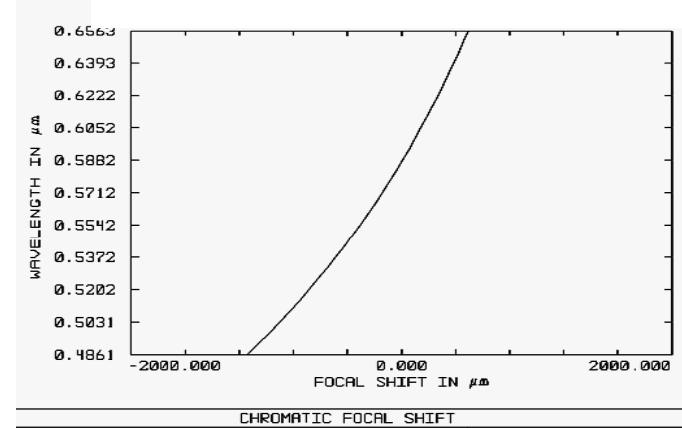
$$0.656 \mu\text{m}$$

$$0^\circ$$

$$13.57^\circ$$

$$19.10^\circ$$

$$23.40^\circ$$



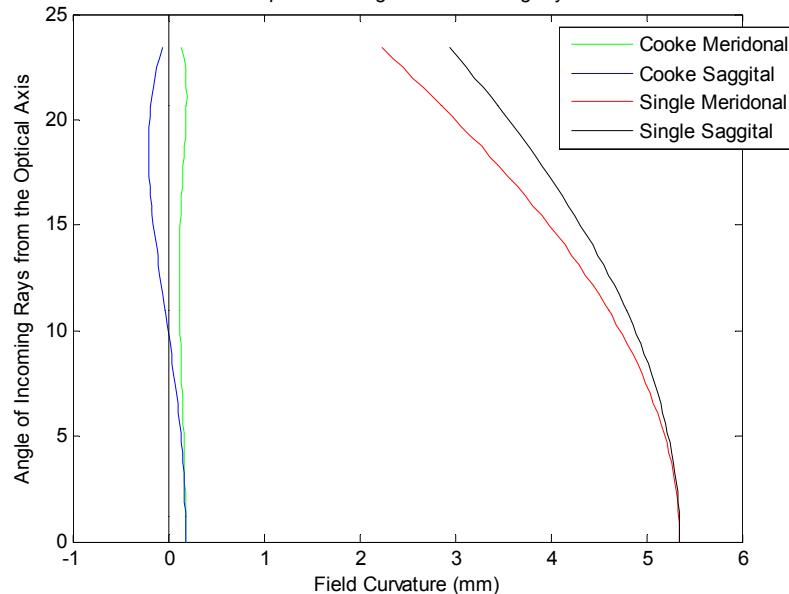
Chromatic  
Aberration

CHROMATIC FOCAL SHIFT

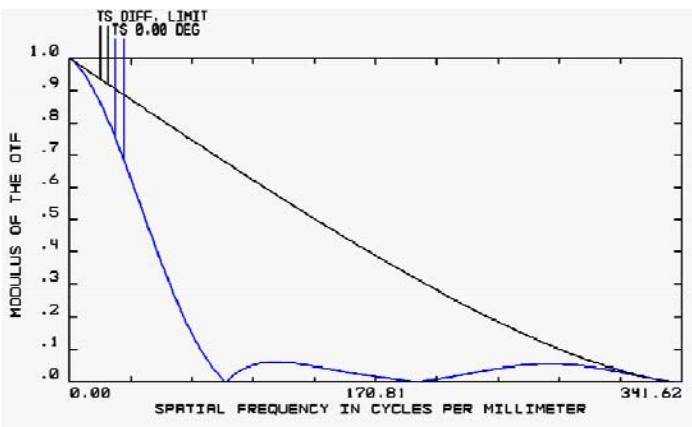
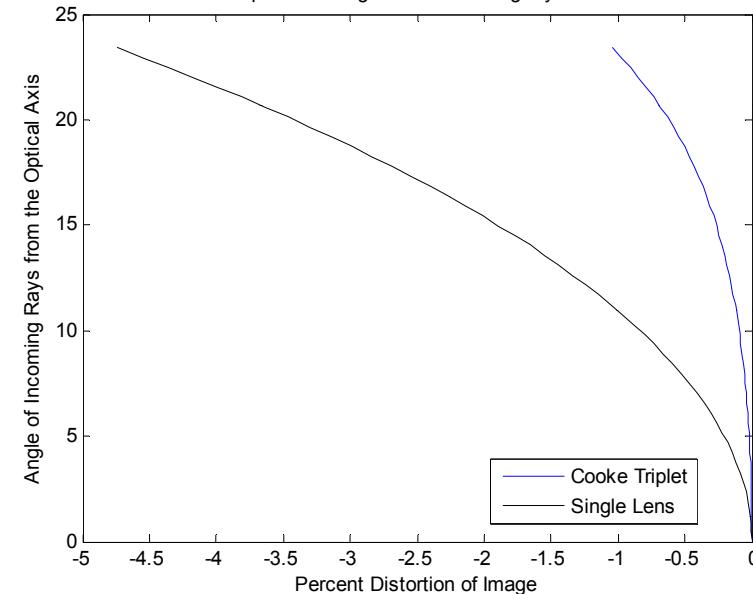
CHROMATIC FOCAL SHIFT

# Cooke Triplet vs. Single Lens

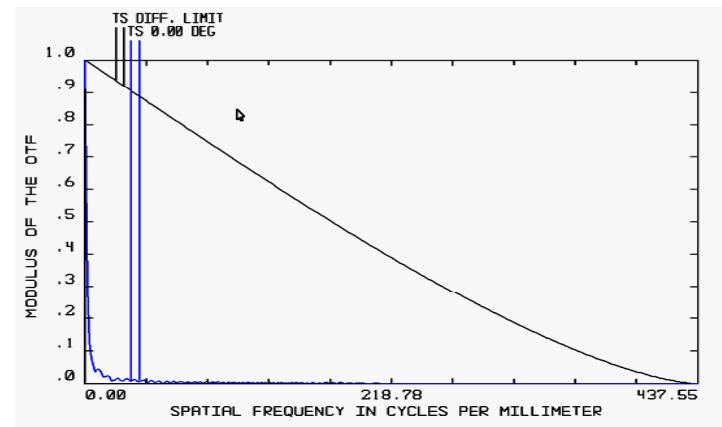
Field Curvature for a Cooke Triplet and Single Lens focusing rays 60mm behind last surface



Distortion for a Cooke Triplet and Single Lens Focusing rays 60mm behind last surface

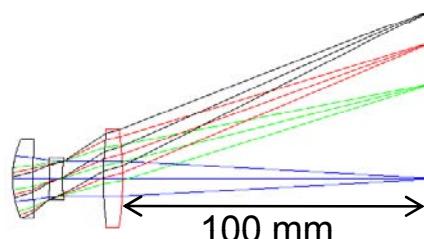


Modulation  
Transfer  
Function

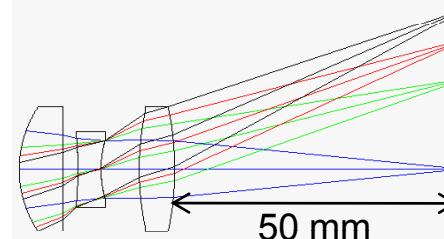
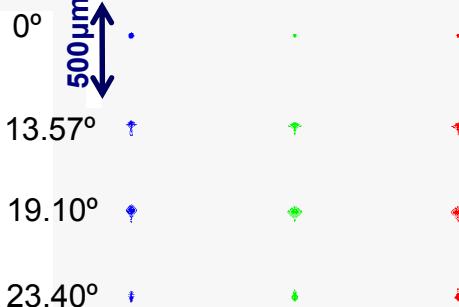


# Cooke Triplet (ID=100, 50, 30mm) : Different image distances

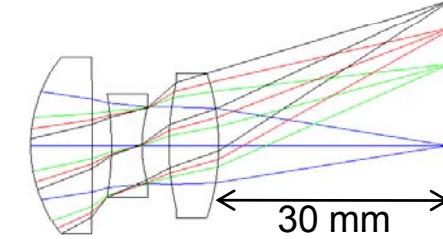
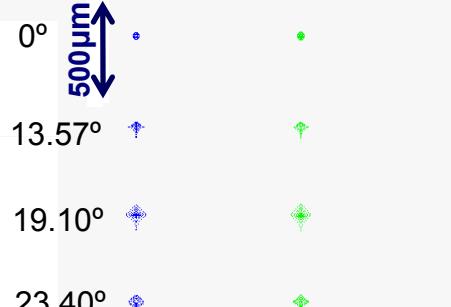
2D layout



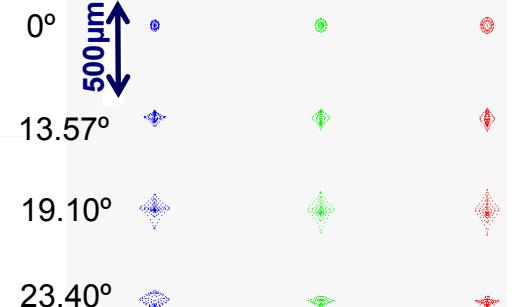
Wavelength 0.486  $\mu\text{m}$  0.588  $\mu\text{m}$  0.656  $\mu\text{m}$



Wavelength 0.486  $\mu\text{m}$  0.588  $\mu\text{m}$  0.656  $\mu\text{m}$

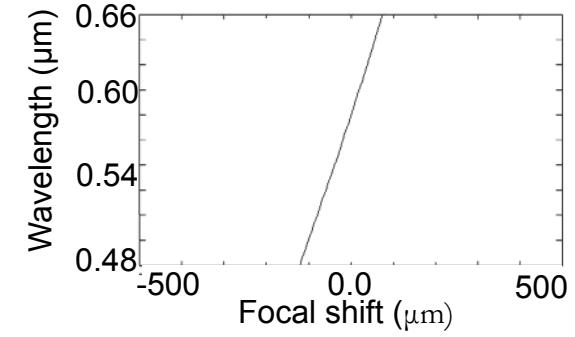
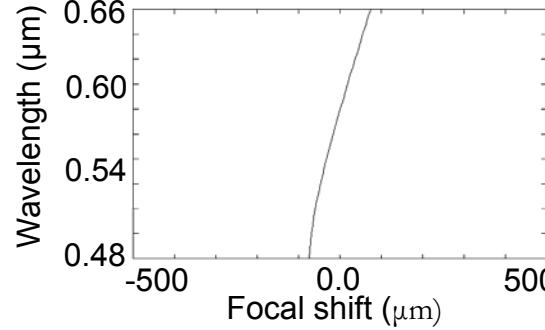
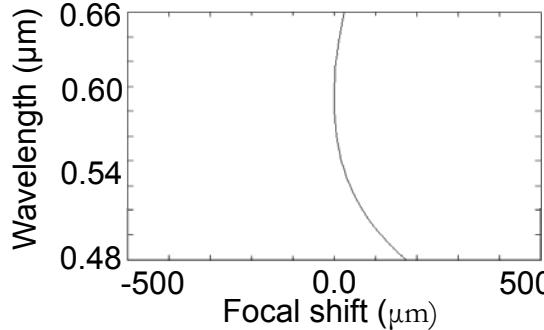


Wavelength 0.486  $\mu\text{m}$  0.588  $\mu\text{m}$  0.656  $\mu\text{m}$



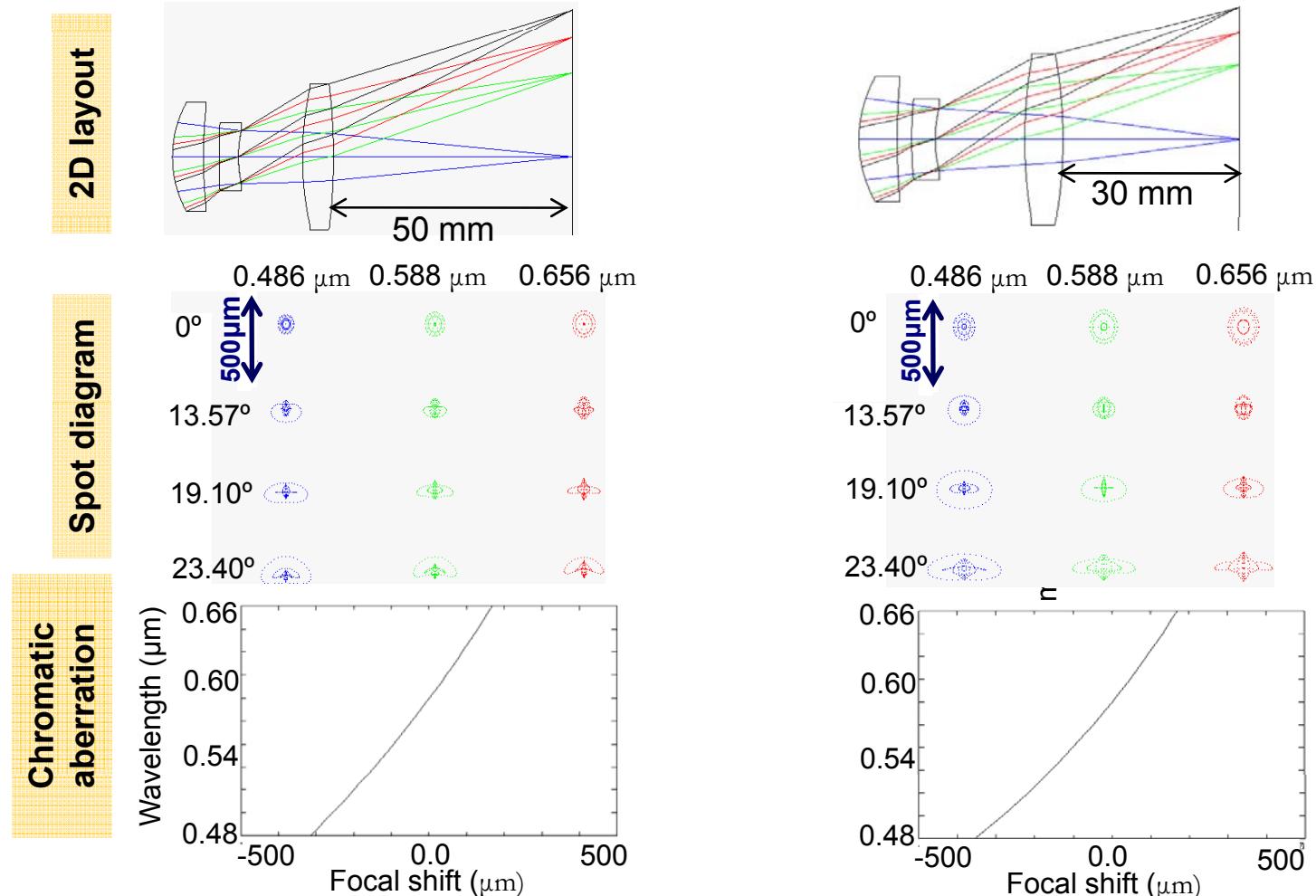
Spot diagram

Chromatic aberration



- ✓ 11 variables (glass choice is fixed), infinity object
- ✓ Shorter image distance: Thicker lens and short distance between positive and negative lenses
- ✓ Large spot and aberration from short focal length

# Cooke Triplet (ID=50, 30mm) : Lens thickness limitation



- ✓ 8 variables (glass choice and lens thickness is fixed), infinity object
- ✓ Lens thickness : 2 positive lens (6.5 mm), and 1 negative lens (4 mm)
- ✓ Lens thickness is very critical to decrease aberration (cannot ignore in optimization)
- ✓ Thickness constraint increases the distance between negative and 2<sup>nd</sup> positive lens

# Glass Optimization

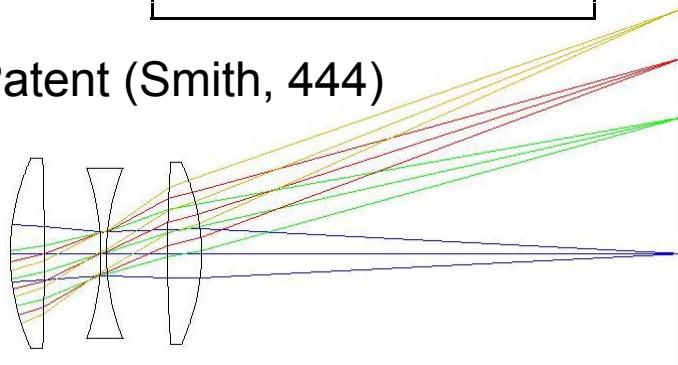
Constant distances and minimal changes to curvatures:

Glass	n	V-value
SK4	1.61	58.62
FN11	1.62	36.17
SK4	1.61	58.62

Optimization

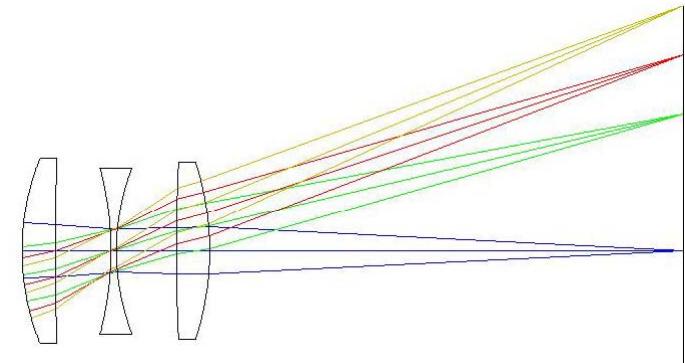
Glass	n	V-value
LAK33	1.75	52.43
BASF2	1.62	30.97
LAK33	1.75	52.43

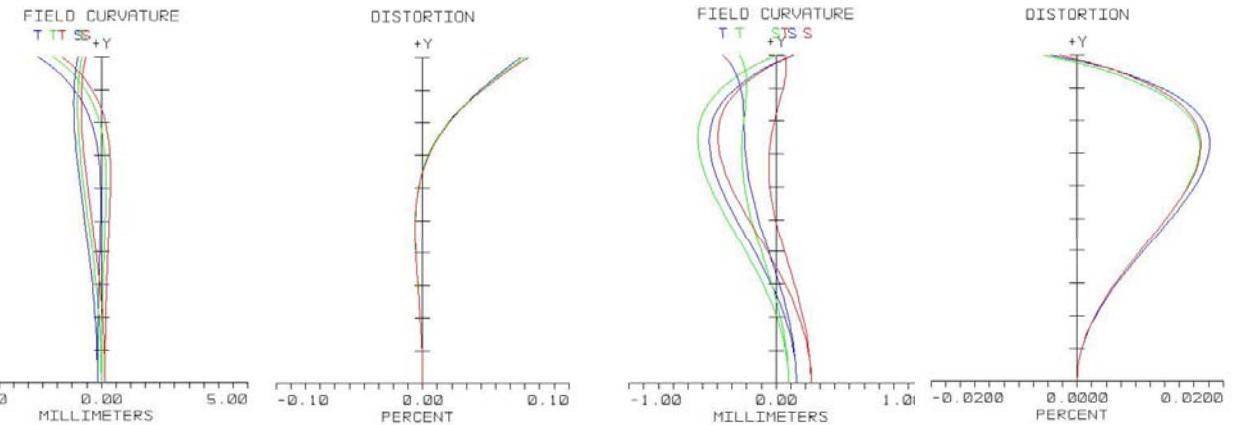
Patent (Smith, 444)



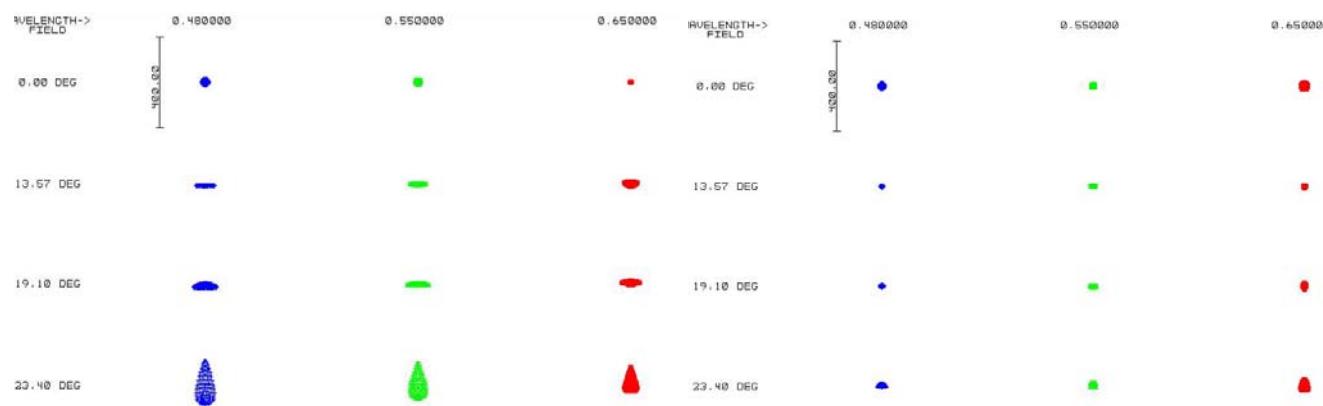
Surf	Radius	Thickness	Diameter
1	40.1	6.0	33.4
2	-537.0	10.0	33.4
3	-47.0	1.0	30.0
4	40.0	10.8	30.0
5	234.5	6.0	32.0
6	-37.9	85.3	32.0

- Negative element with same n and higher dispersion.
- Positive element with higher n and higher dispersion.

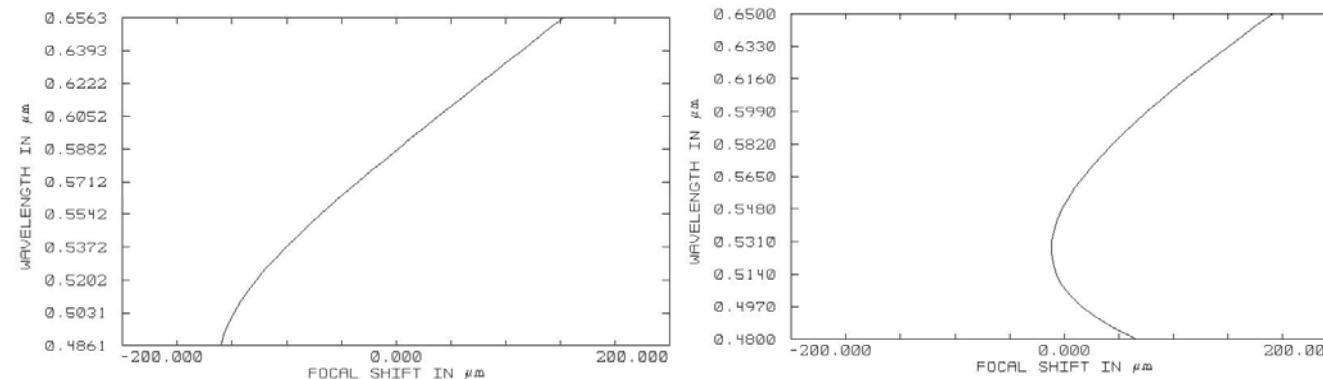




- Increase in ( $n_{\text{crown}} - n_{\text{flint}}$ ) reduces field curvature and distortion.



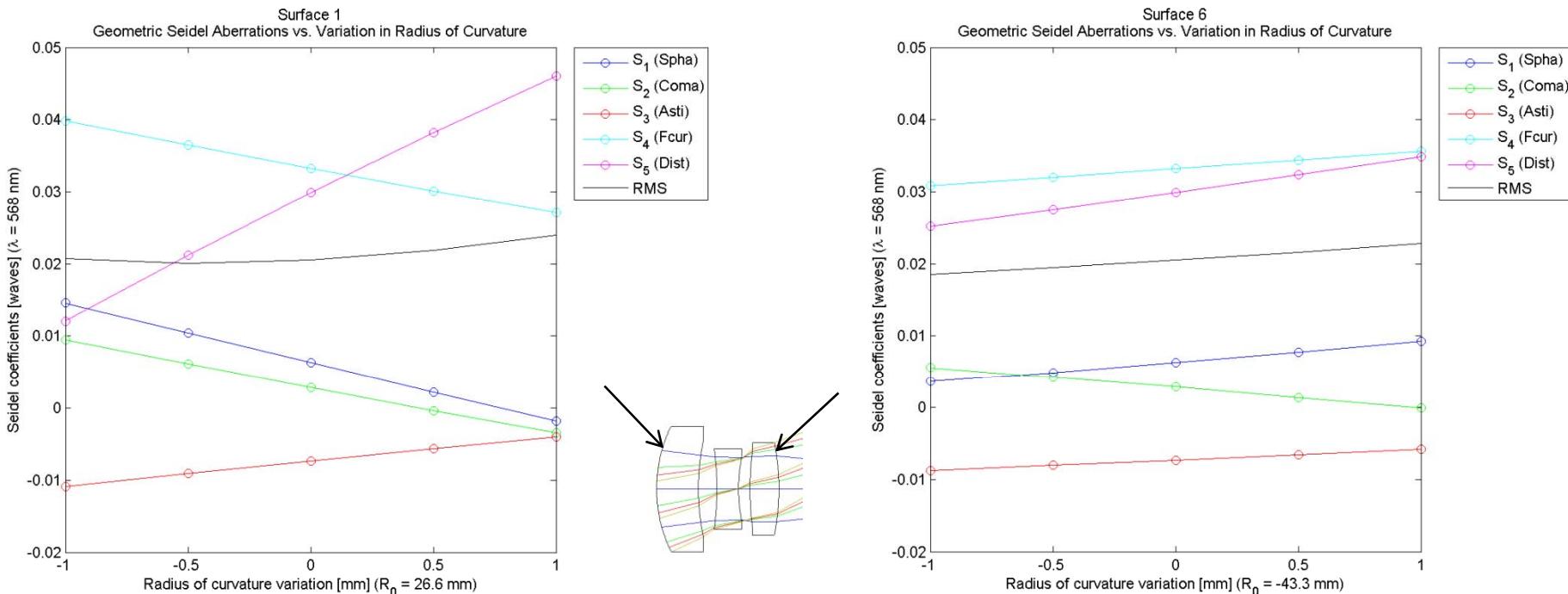
- Increase in ( $n_{\text{crown}} - n_{\text{flint}}$ ) reduces astigmatism and coma.



- Increase in ( $n_{\text{crown}} - n_{\text{flint}}$ ) reduces chromatic aberration.

# Variations from optimal design (1)

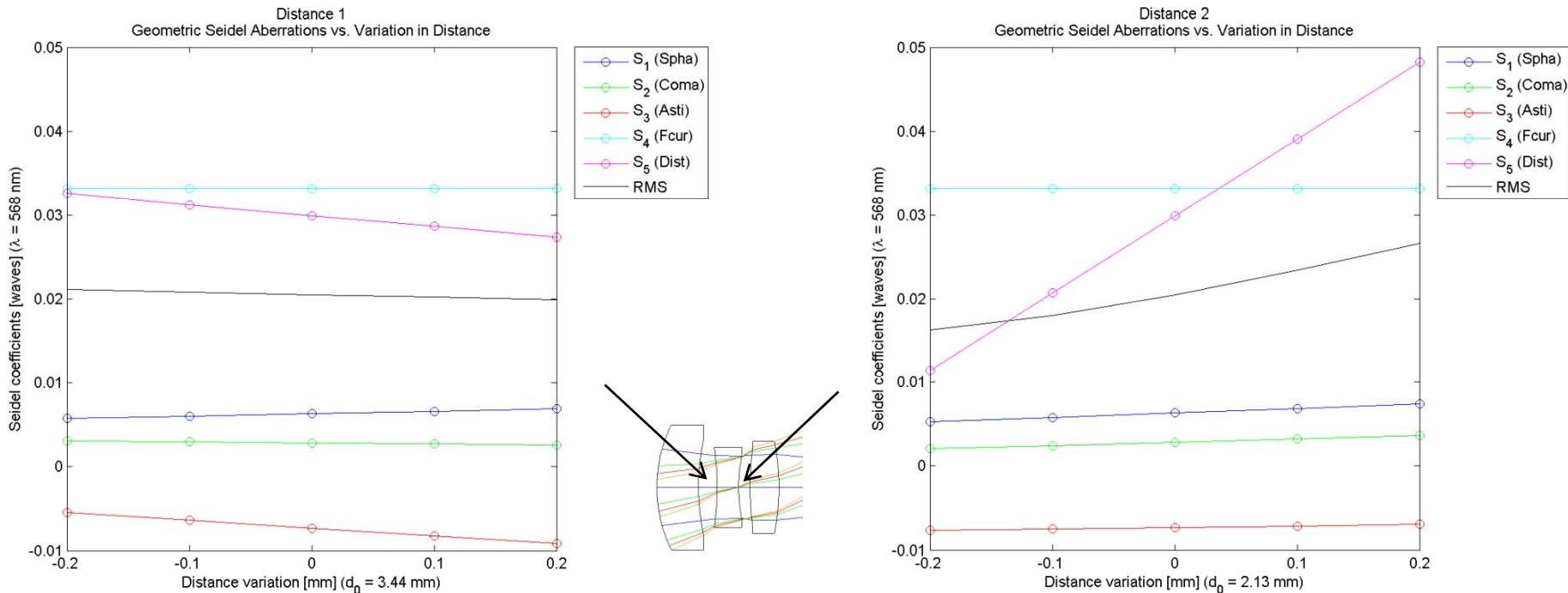
- From the optimized triplet, varied each surface's radius of curvature slightly ( $\pm 1$  mm) to determine effect of a given surface on aberrations



- First lens is relatively highly curved → contribution to distortion is pronounced
- Also considerably more sensitivity in first lens for spherical aberration, coma, and field curvature
- Aberrations nearly at a minimum for 1<sup>st</sup> surface (not so for other lenses); first surface adds the bulk of the aberrations, Zemax will force this surface to a minimum so that “downstream” lenses have less to correct

# Variations from optimal design (2)

- Also changed the spacing between the lenses ( $\pm 0.2$  mm) to represent possible challenges with alignment in real systems



- Greater sensitivity to perturbations in the spacing between second and third lenses ("Distance 2"), particularly distortion.
- Note that field curvature is unchanged by variations in distance; due to the fact that field curvature depends on lens power (and focal length), not on lens placement

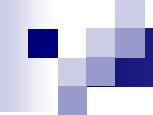
# Conclusions and Future Work

- The first lens in the triplet introduces the majority of the aberrations, the subsequent lens attempt to correct
- Making the first lens aspheric and/or compound to correct some of this initial aberrations could improve the triplet performance further
- Due to the interdependence of all the variables, a large number of iterations ( $\sim 10^9$ ) are required to find the ‘best’ configuration
- The Cooke triplet greatly reduces the Seidel aberrations while maintaining a relatively large aperture (F/8)



# References:

- Smith, W. J. (2007). *Modern optical engineering*. New York, NY: McGraw-Hill Professional.
- Kidger, M. (2001). *Fundamental optical design*. Bellingham, WA: SPIE Publications.
- Goodman, J. W. (1968). *Introduction to Fourier Optics*. San Francisco, CA: McGraw-Hill.
- Taylor, H. D. (1895). *Lens*. Patent No. 540,122, United States Patent Office.



# **SUPPLEMENTAL INFORMATION**

# Zemax- model, optimize and analyze the design of optical systems

Screenshot of Zemax software interface showing a lens design and optimization process.

**Top Bar:**

- File Editors System Analysis Tools Reports Macros Extensions Window Help
- Buttons: New Open Save SAS Upd Gen Fie Wav Lay L3d Ray Optd Fcd Spt Mtf Fps Enc Opt Ham Tol Gla Len Sys Pre Chk

**Lens Data Editor:**

Surf:	Type	Comment	Radius	Thickness	Glass	Semi-Diameter	Conic
OBJ	Standard		Infinity	Infinity		Infinity	0.00000
1	Standard		26.585199 V	7.736537 V	N-LASF31 S	11.676172	0.00000
2	Standard		43.429037 V	3.435887 V		8.940243	0.00000
3	Standard		-55.415591 V	3.999980 V	SF14 S	7.469473	0.00000
STO	Standard		29.198443 V	2.127319 V		6.034548	0.00000
5	Standard		55.521418 V	5.365190 V	N-LASF31 S	7.457009	0.00000
6	Standard		-43.266572 V	60.000000		8.594248	0.00000
IMA	Standard		Infinity	-		30.482764	0.00000

**3D Layout View:**

I: Layout Z = 78.77, Y = 24.94

**Merit Function Editor:**

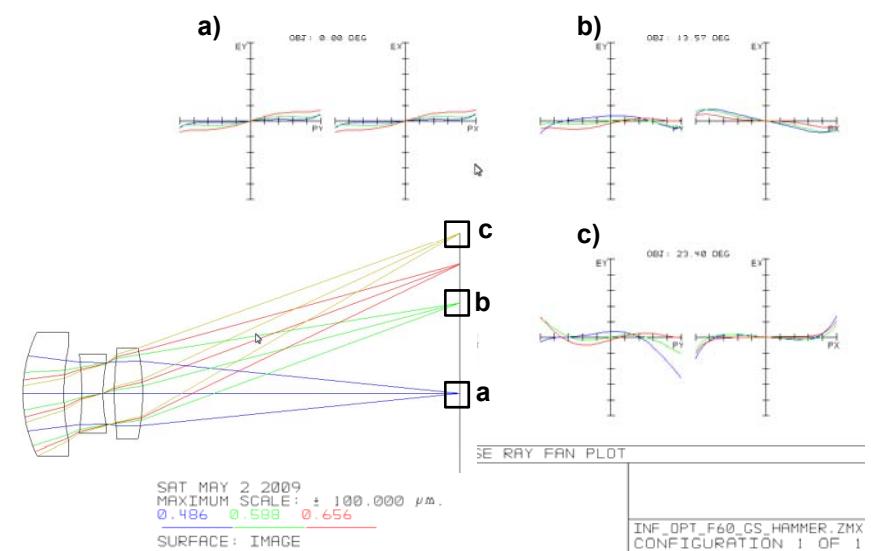
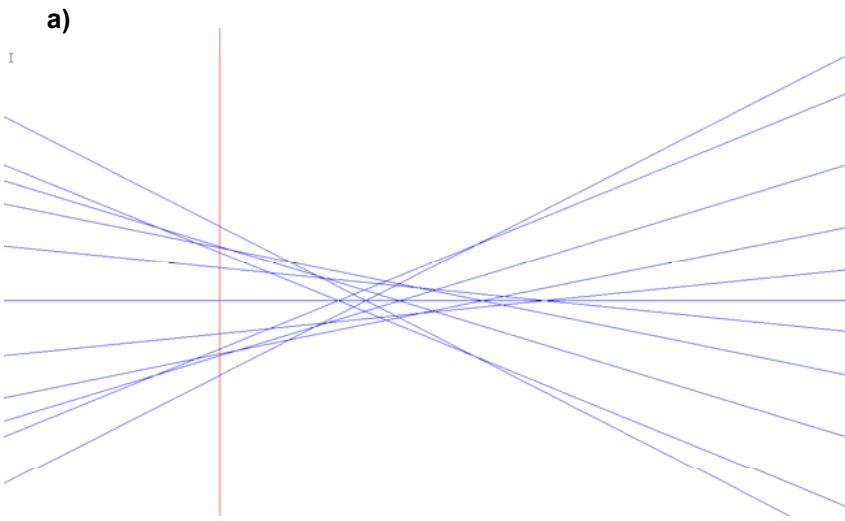
Merit Function Editor: 4.469931E-003

Oper #	Type	Target	Weight						
1 DMFS	DMFS								
2 BLNK	BLNK	Default merit function: RMS spot radius centroid CQ 3 rings 6 arms							
3 BLNK	BLNK	Default air thickness boundary constraints.							
4 MNCA	MNCA	1	6	2.000000	1.000000	2.000000	0.000000		
5 MXCA	MXCA	1	6		100.000000	1.000000	100.000000	0.000000	
6 MNEA	MNEA	1	6		2.000000	1.000000	1.999972	2.820996E-004	
7 BLNK	BLNK	Default glass thickness boundary constraints.							
8 HNCG	HNCG	1	6	4.000000	1.000000	3.999980	1.416022E-004		
9 MXCG	MXCG	1	6		18.000000	1.000000	18.000000	0.000000	
10 MNEG	MNEG	1	6		4.000000	1.000000	3.999992	2.127376E-005	
11 BLNK	BLNK	Aberration Optimization							
12 COMA	COMA	7	2	0.000000	1.000000	0.000000	0.000000		
13 SPHA	SPHA	7	2	0.000000	1.000000	0.000000	0.000000		
14 FCUR	FCUR	7	2	0.000000	1.000000	0.000000	0.000000		
15 DIST	DIST	7	2	0.000000	1.000000	0.000000	0.000000		
16 ASTI	ASTI	7	2	0.000000	1.000000	0.000000	0.000000		
17 BLNK	BLNK								
18 BLNK	BLNK	Operands for field 1.							
19 TRAC	TRAC	1	0.000000	0.000000	0.335711	0.000000	0.072722	2.056060E-003	0.108802

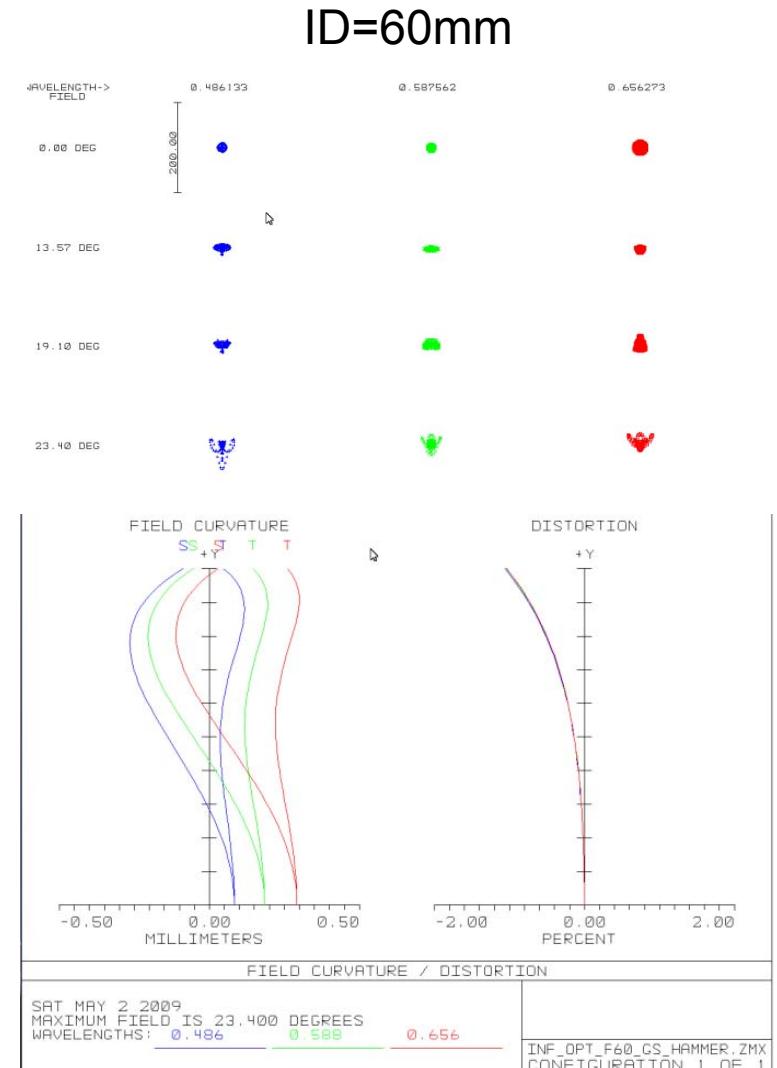
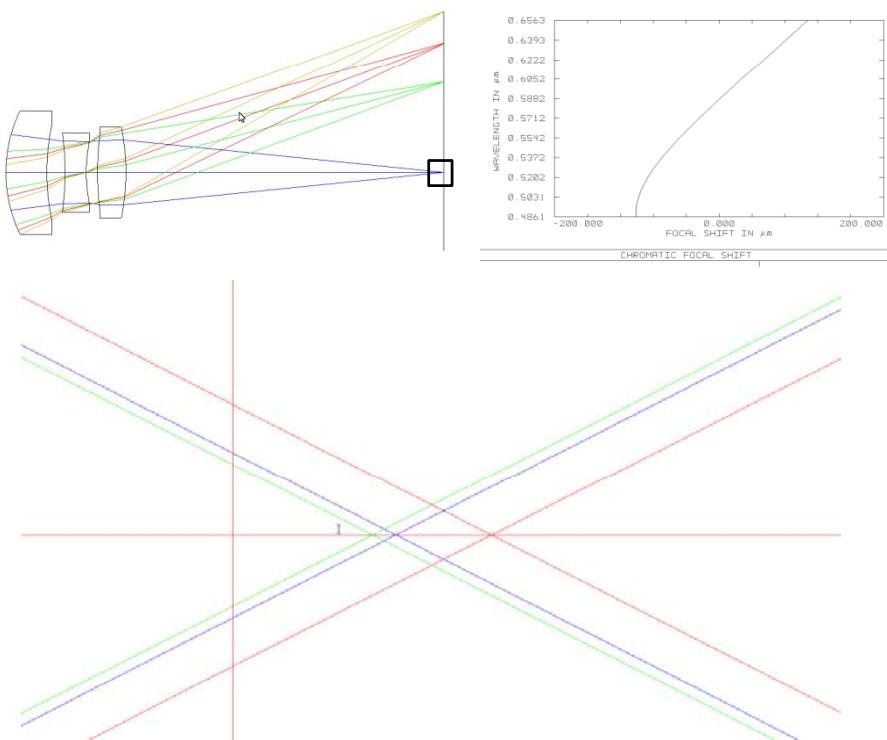
**Bottom Taskbar:**

- Buttons: Off Plane, Ray Fan, Report Gr., Sequence, Focal Shift, 3D Layout, Field Curv., Matrix S., Wavefront...
- Start button
- System icons
- Time: 2:14 PM

# Ray Diagrams and Ray Fan

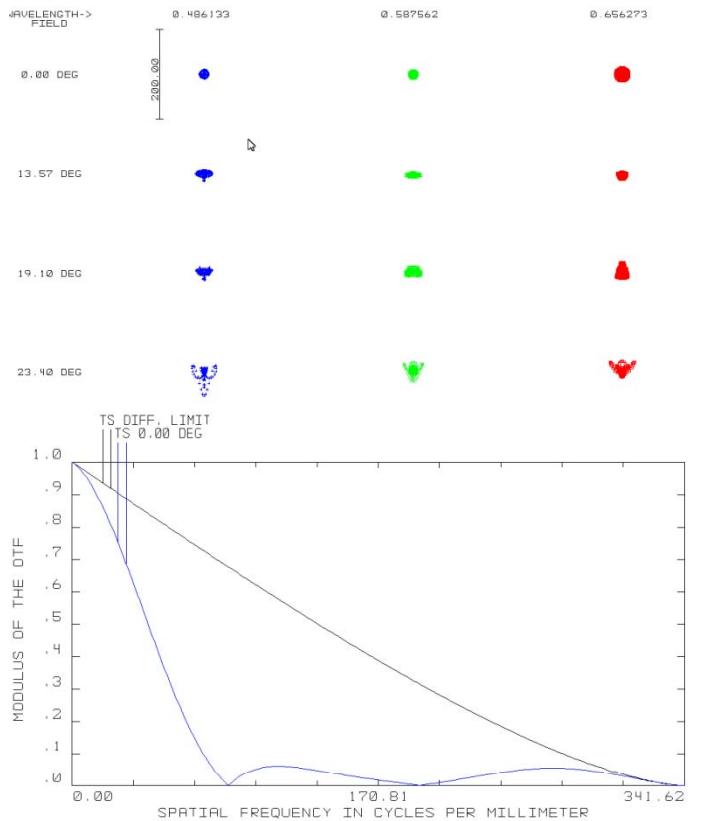


# More on Chromatic Abberations

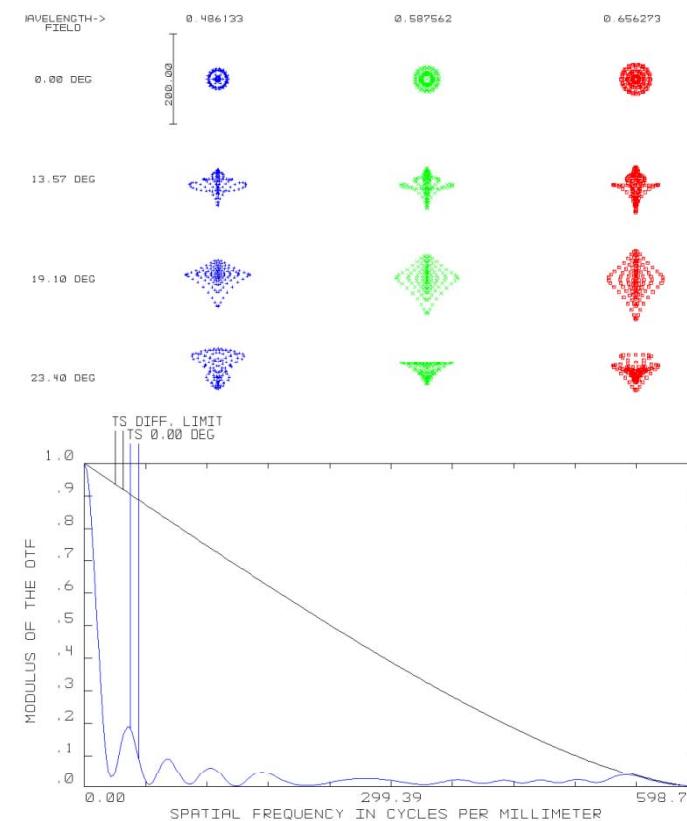


# Comparison of ID=60mm and ID=20mm Triplet

ID=60mm

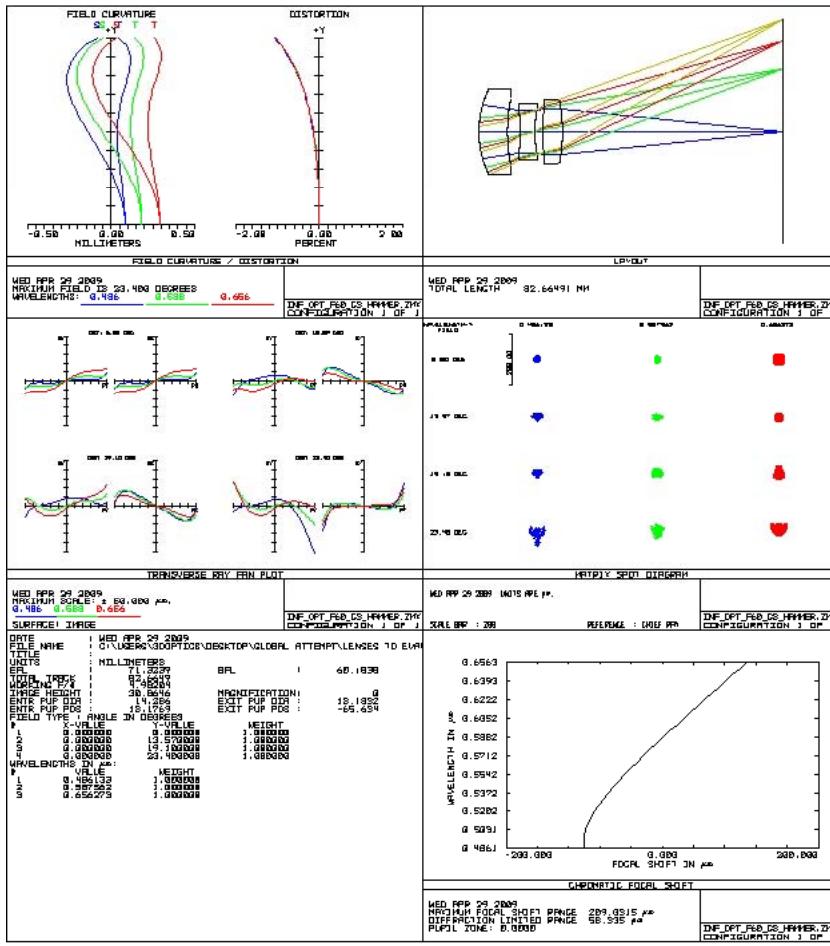


ID=20mm

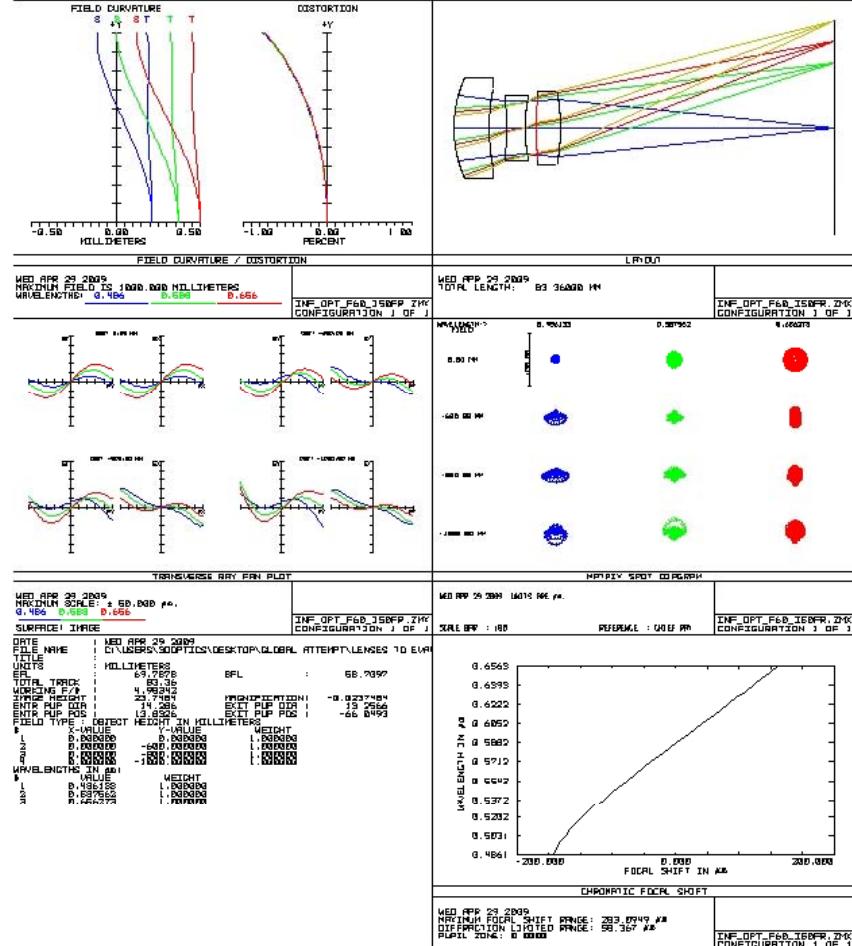


# Objects at Finite Distances

OD= Infinity

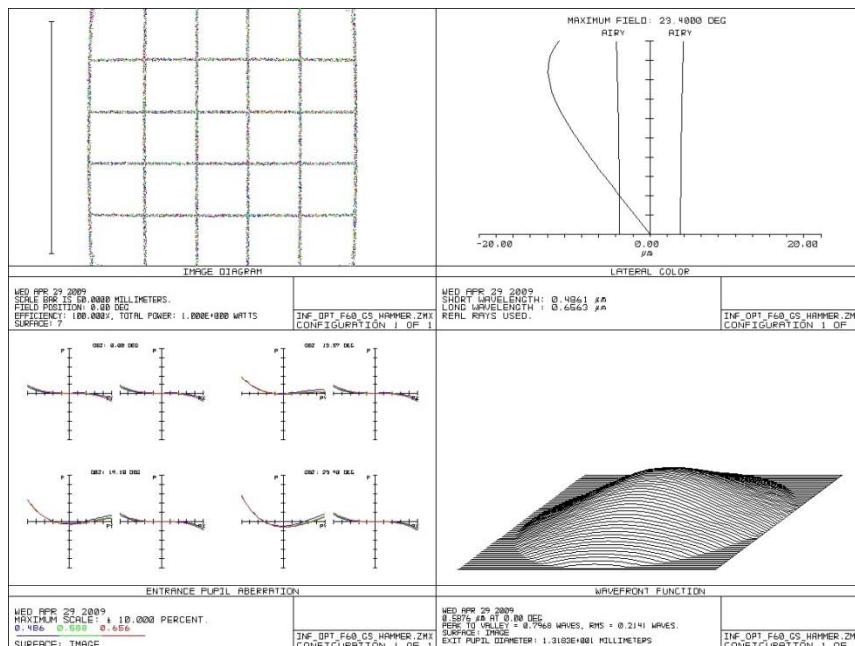


OD= 50xID

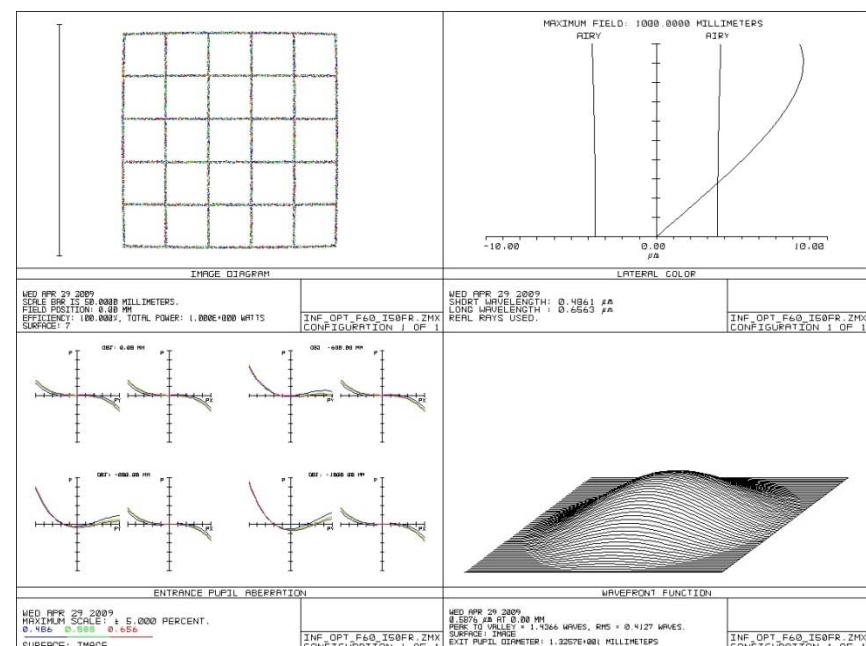


# Objects at Finite Distances

OD= Infinity

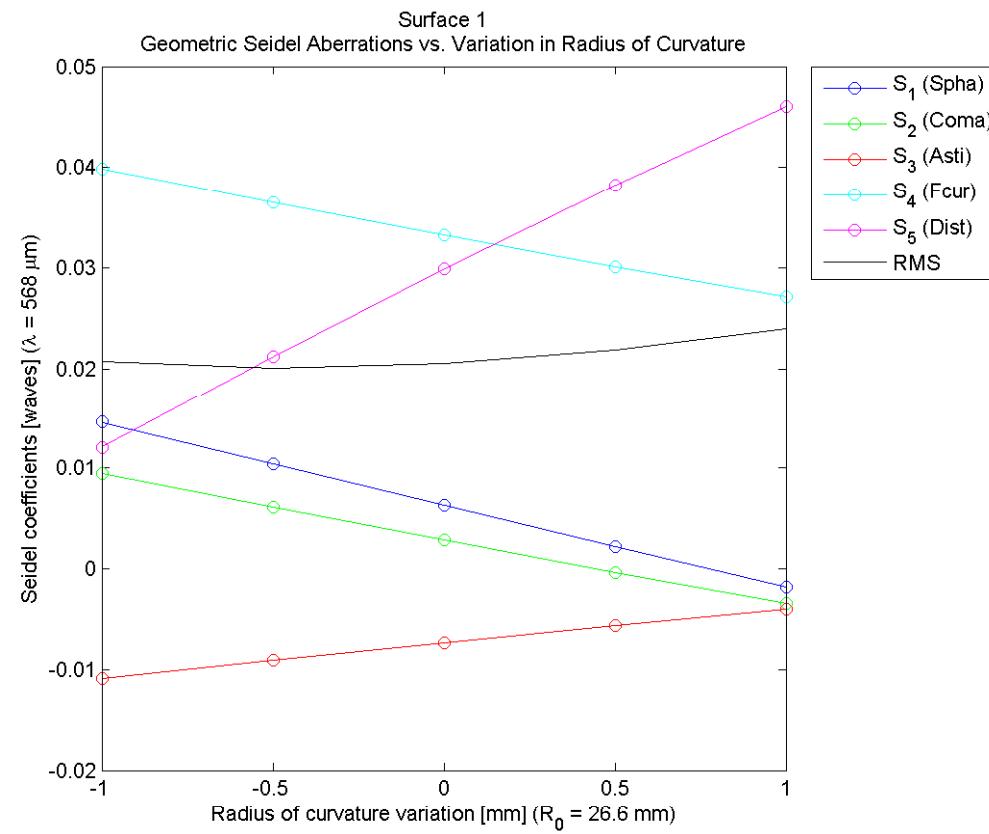


OD= 50xID



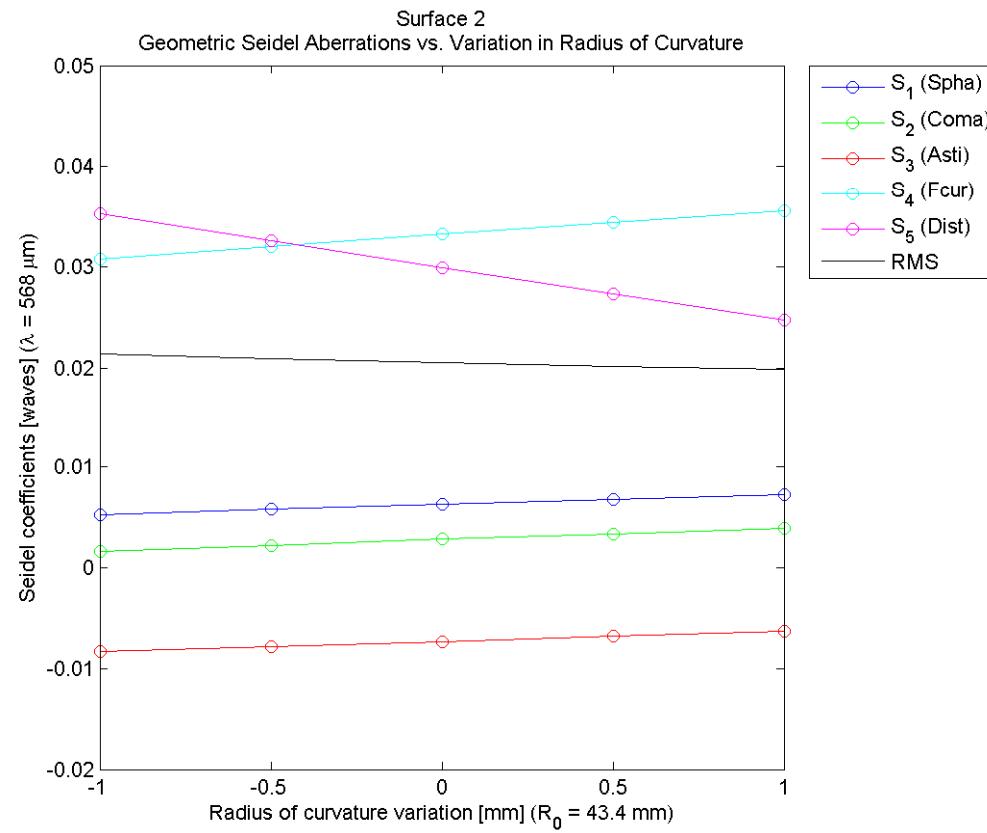
# Variations from optimal design

## ■ Surface 1



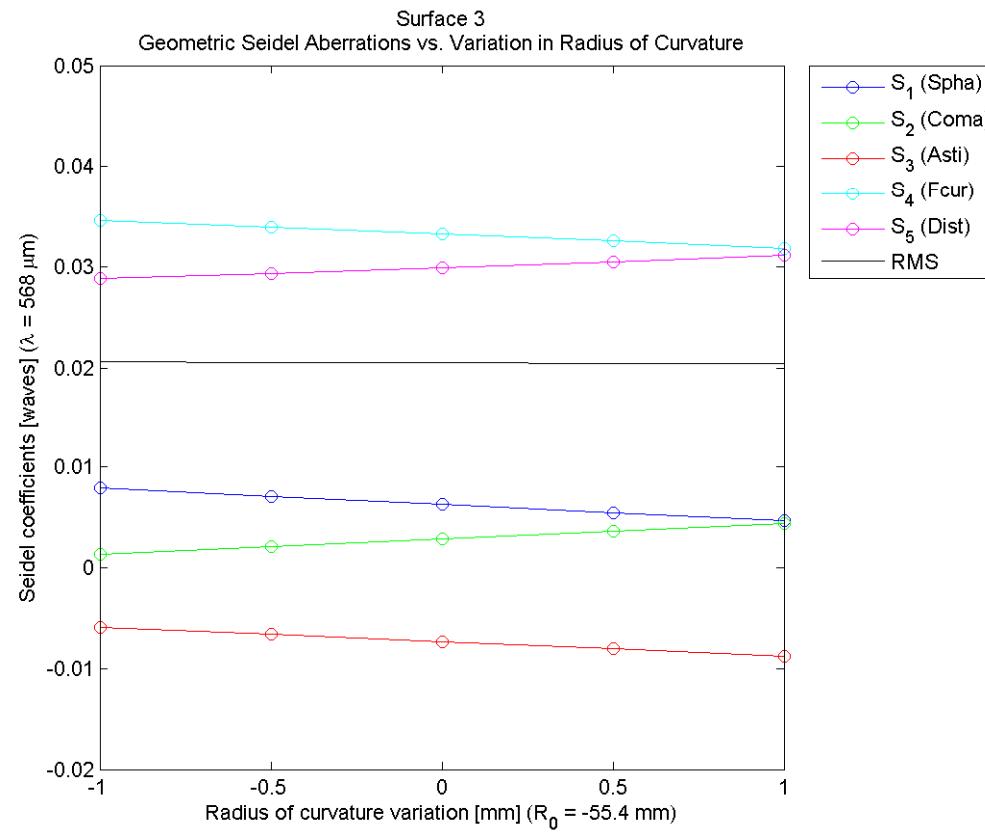
# Variations from optimal design

## ■ Surface 2



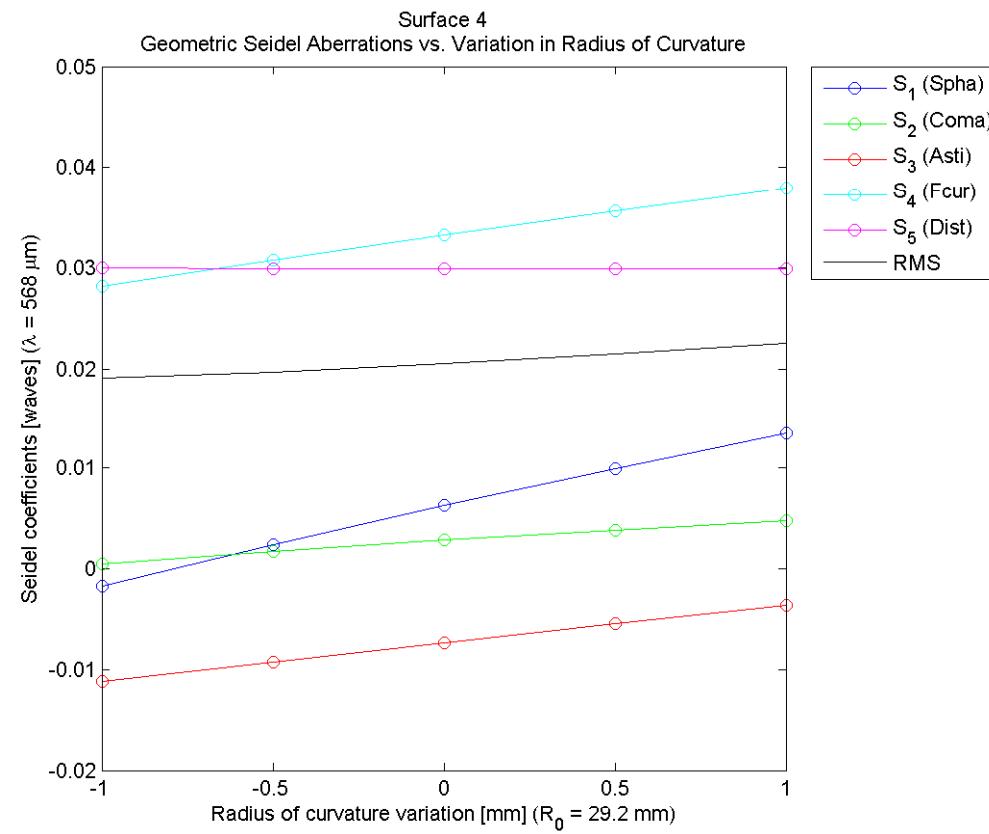
# Variations from optimal design

## ■ Surface 3



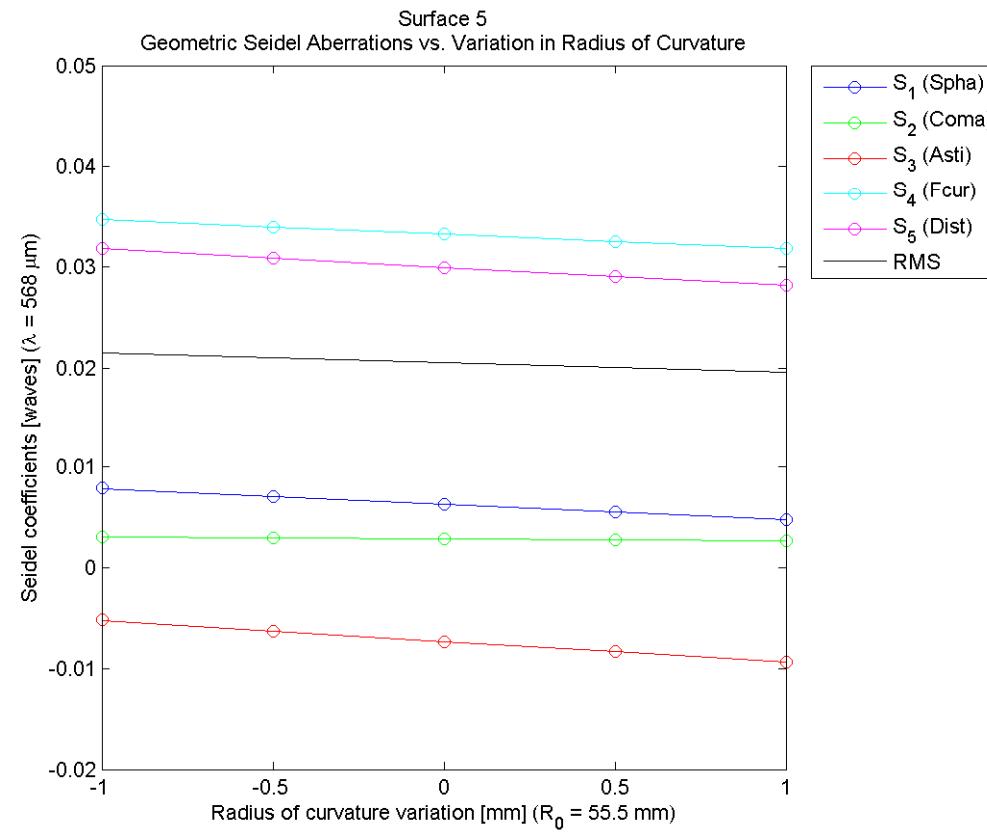
# Variations from optimal design

## ■ Surface 4



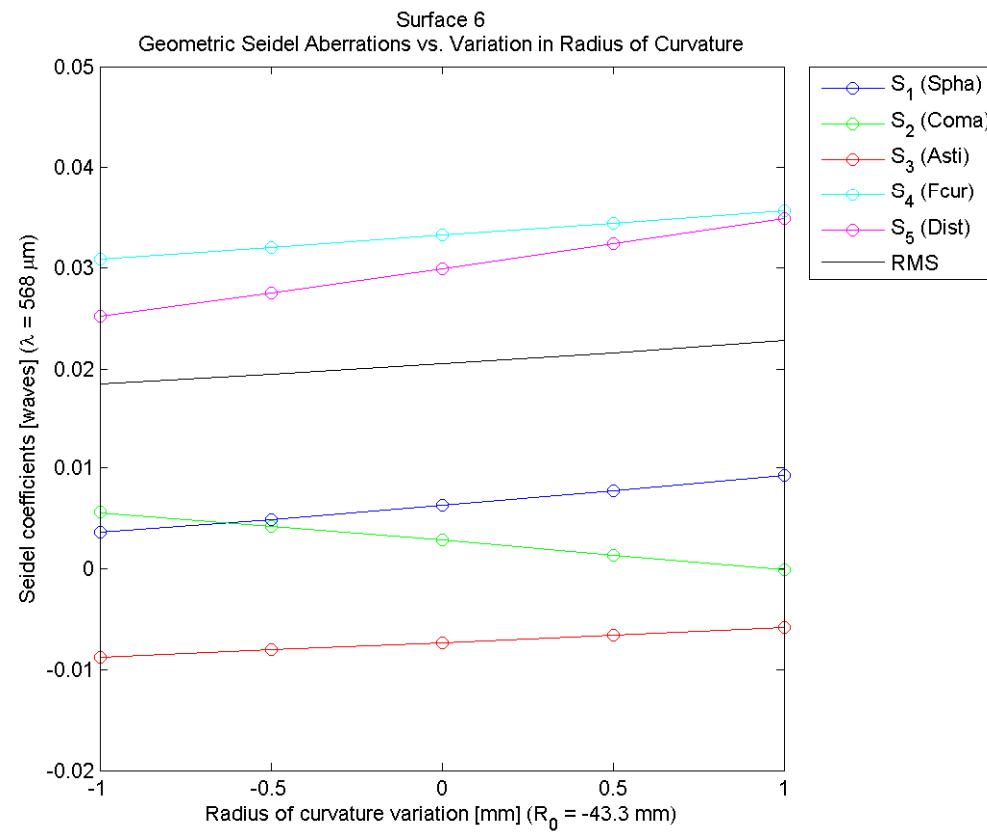
# Variations from optimal design

## ■ Surface 5



# Variations from optimal design

## ■ Surface 6



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