

# 3.40 LECTURE SUMMARY - Nov 9th

11/ 16/ 2009

# INTRODUCTION

- Precipitation Hardening
  - It relies on changes in solid solubility with temperature to produce a second phase
- Hardening Mechanisms
  - Modulus Mismatch
    - Changes the dislocation energy
  - Ordered Precipitates
  - Size Effect
    - Cutting to Bowing Transition
    - Coherent and Incoherent Precipitates

# 2 COMPONENT PHASE DIAGRAMS

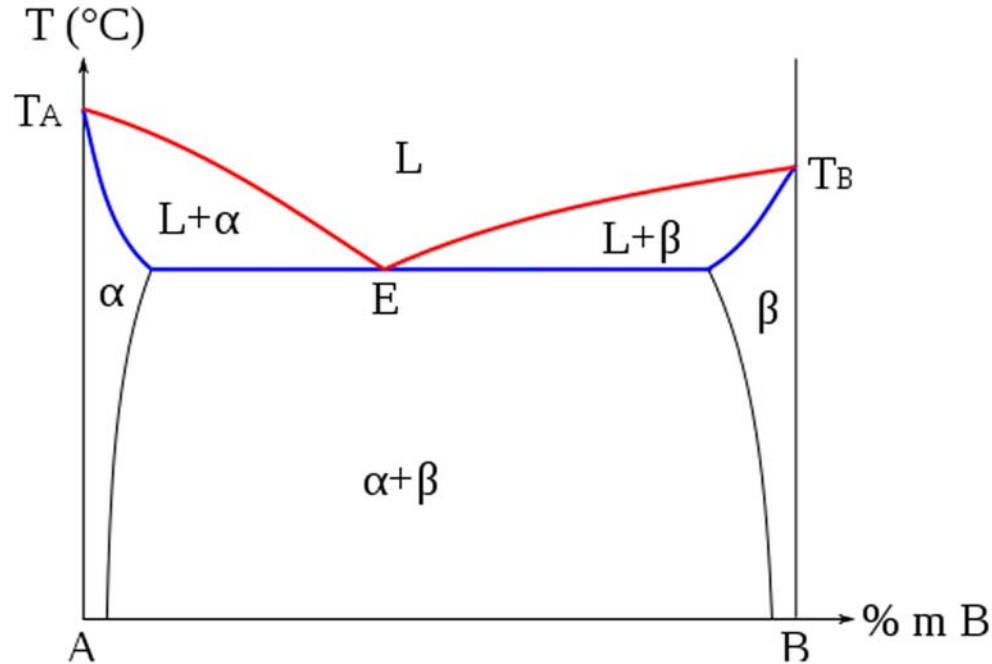
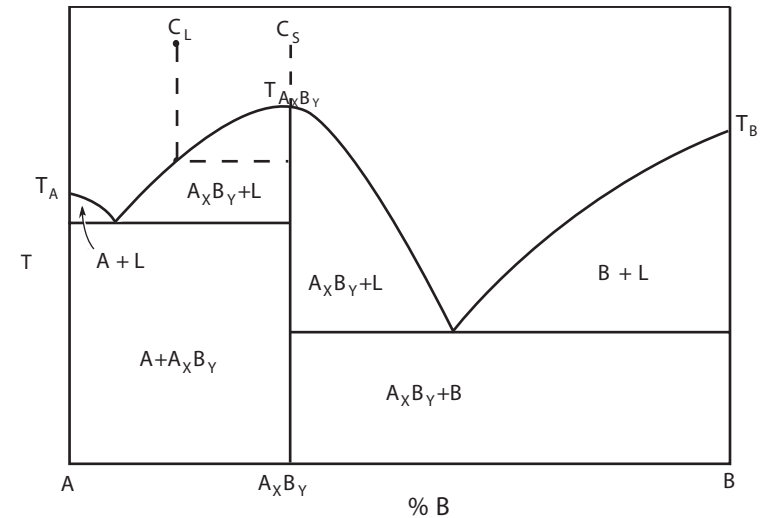


Fig. 1: System forming 2 Solid Solutions  
[[http://en.wikipedia.org/wiki/Phase\\_diagram](http://en.wikipedia.org/wiki/Phase_diagram)]



Courtesy of Lionel C. Kimerling. Used with permission.

Fig. 2: System forming an Intermetallic  
[<http://www.substech.com/>]

# ANTI-PHASE BOUNDARIES

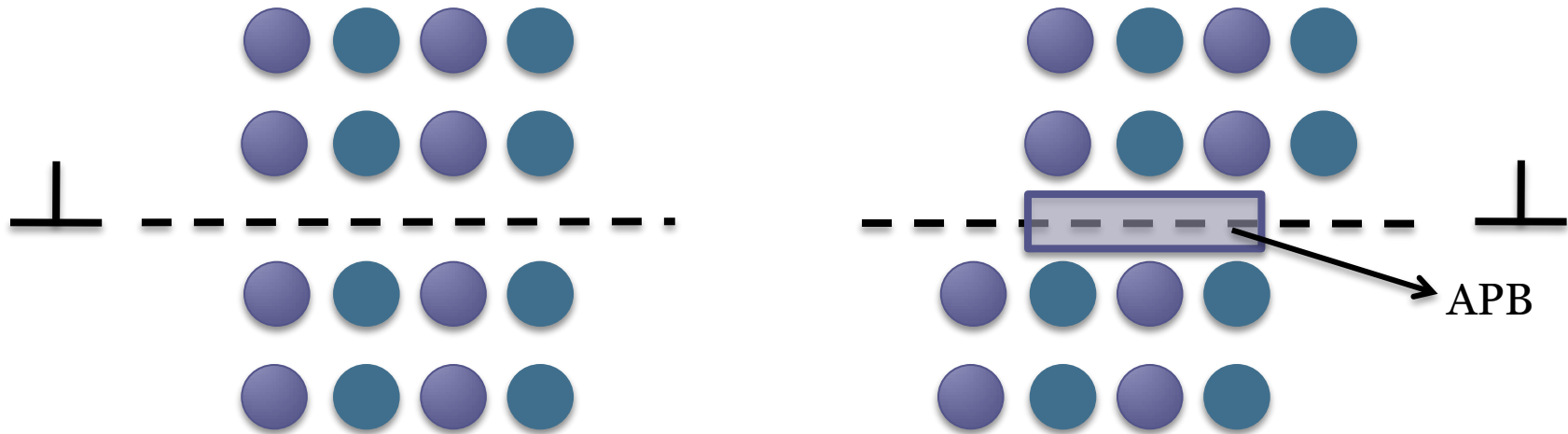


Fig. 3: Dislocation cutting through an ordered precipitate forming an APB

- Additional energy is required to create an APB

$$\Delta\tau_{APB} = \frac{\pi}{2b} \gamma_{APB} \frac{r}{L} = \frac{\pi}{2b} \gamma_{APB} V_f$$

# PRECIPITATION HARDENING

- Contributions to Precipitation Hardening
  - Anti-Phase Boundaries
  - Interfaces
  - Coherency Strains
  - Modulus Effect



**Decreasing effect on Strength**

$$\Delta\tau_{tot} = \Delta\tau_{APB} + \Delta\tau_{int} + \Delta\tau_{coh} + \Delta\tau_{mod}$$

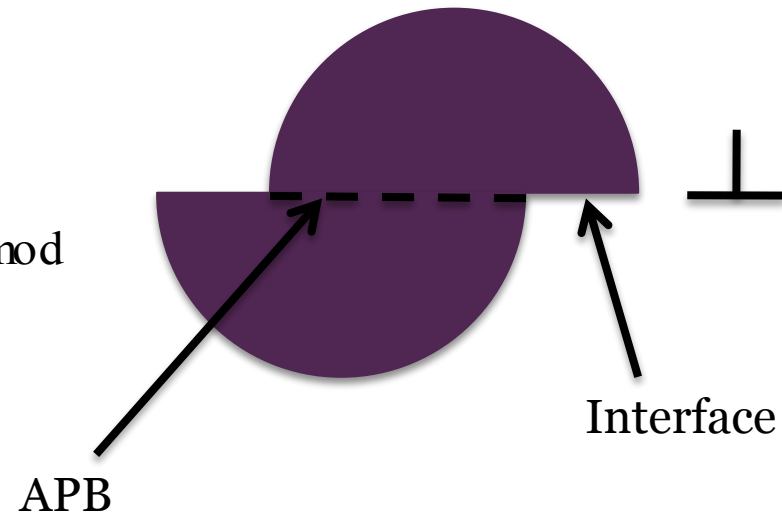


Fig. 4: Schematic of a sheared precipitate

# SIZE EFFECTS

- As the size of the second phase particle increases
  - Cutting through it becomes more difficult

$$\Delta\tau_{cutting} \propto r$$

- Dislocations tend to bow around the particle by Orowan Looping

$$\Delta\tau_{bowing} \propto \frac{1}{r}$$

- Critical radius  $\sim 5 - 30$  nm

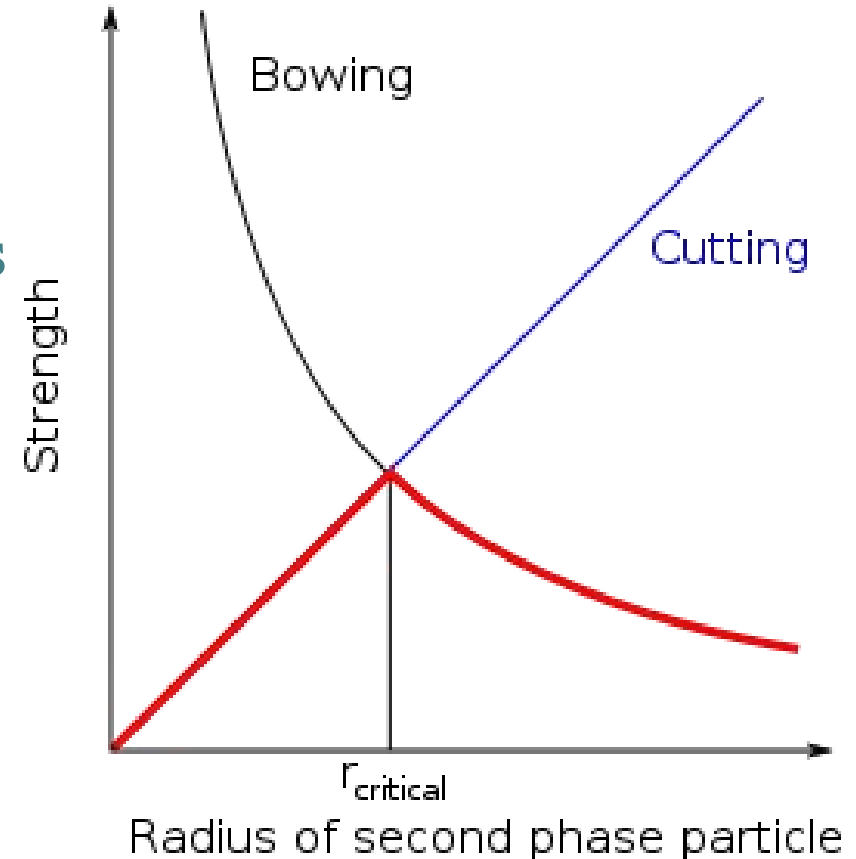
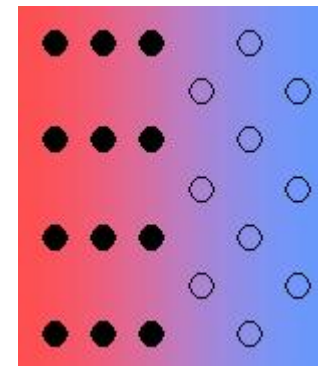


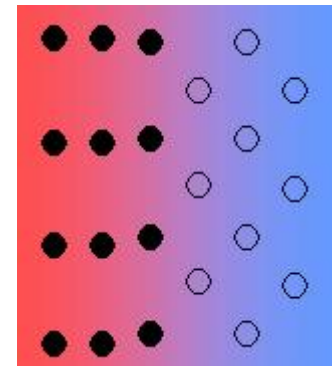
Fig. 5: Shear Strength vs. Particle Radius  
[[http://en.wikipedia.org/wiki/Precipitation\\_strengthening](http://en.wikipedia.org/wiki/Precipitation_strengthening)]

# SIZE EFFECTS

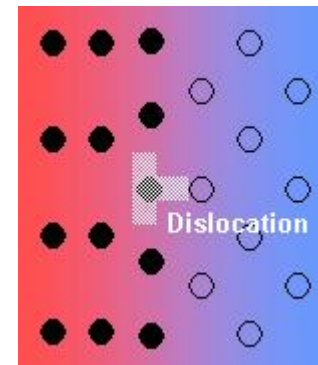
- As the size increases, coherent particles transform to incoherent precipitates
- The strain energy is reduced and the strengthening effect is weakened
- The critical radius for this transition  $\sim 10 \text{ nm} - 1 \mu\text{m}$



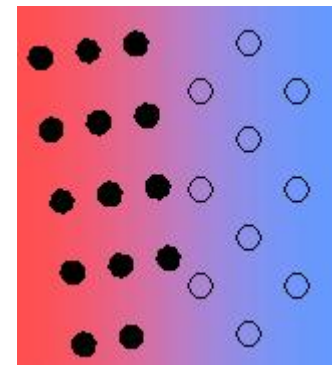
(a) Coherent



(b) Coherent with Strain



(c) Semi-Coherent



(d) Incoherent

Fig. 6: Different types of interfaces  
[<http://www.doitpoms.ac.uk/tlplib/solid-solutions/>]

# PRECIPITATE FREE ZONES

- Heterogeneous nucleation at grain boundaries, dislocations
- Particles nucleate at grain boundaries
- Regions surrounding the grain boundary are depleted of solutes, forming PFZs

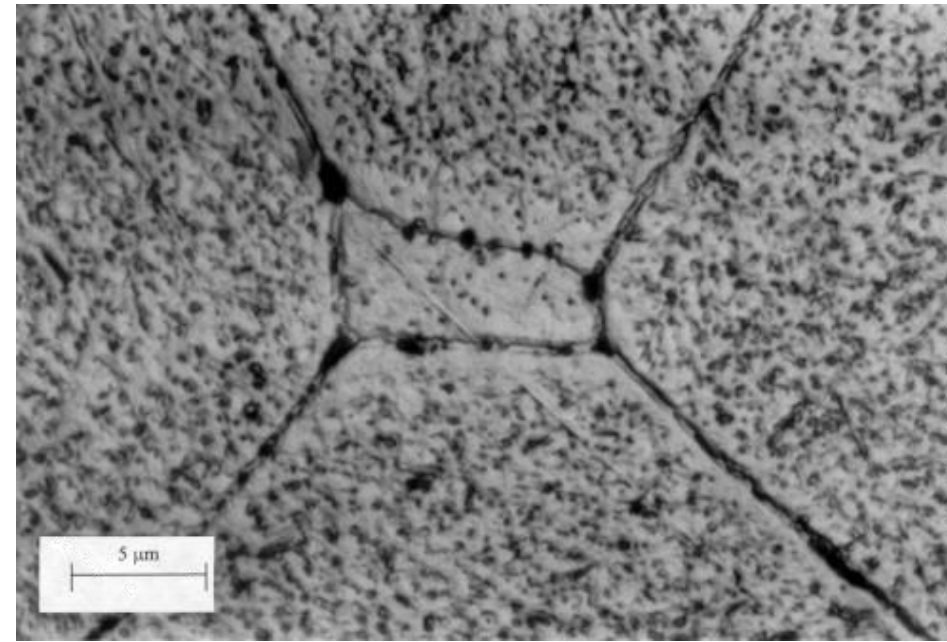


Fig. 7: PFZ near grain boundaries in Al -4 wt% Cu  
[<http://www.msm.cam.ac.uk/phasetrans/abstracts/pfz.html>]



# SUMMARY

- Precipitation Hardening provides a greater increase in strength than solid solution strengthening
- Intermetallics are better obstacles to dislocation motion due to the creation of Anti-Phase Boundaries
- 2 critical radii exist:
  - Cutting to bowing:  $r_c \sim 10 \text{ nm}$
  - Coherent to Incoherent:  $r_{c/i} \sim 10 \text{ nm} - 1 \mu\text{m}$



**QUESTIONS?**

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