

Lecture 14

Last time: $w(t, \tau) \Rightarrow w(t - \tau)$

$$y(t) = \int_{-\infty}^t w(t - \tau)x(\tau)d\tau$$

$$\text{Let: } \begin{cases} \tau' = t - \tau \\ -d\tau = d\tau' \end{cases}$$

$$y(t) = \int_0^{\infty} w(\tau')x(t - \tau')d\tau'$$

For the differential system characterized by its equations of state, specialization to invariance means that the system matrices A, B, C are constants.

$$\dot{\underline{x}} = A\underline{x} + B\underline{u}$$

$$\underline{y} = C\underline{x}$$

For A, B, C constant:

$$\underline{y}(t) = C\underline{x}(t)$$

$$\underline{x}(t) = \Phi(t - t_0)\underline{x}(t_0) + \int_{t_0}^t \Phi(t - \tau)B\underline{u}(\tau)d\tau$$

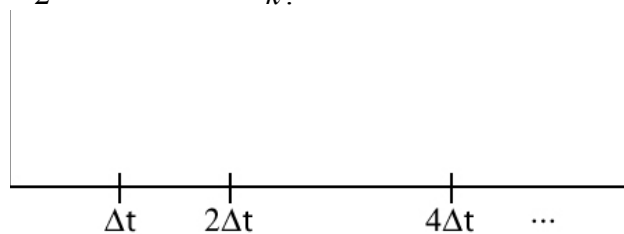
The transition matrix can be expressed analytically in this case.

$$\frac{d}{dt}\Phi(t, \tau) = A\Phi(t, \tau), \quad \text{where } \Phi(\tau, \tau) = I$$

This is a matrix form of first order, constant coefficient differential equation. The solution is the matrix exponential.

$$\Phi(t, \tau) = e^{A(t-\tau)}$$

$$e^{A(t-\tau)} = I + A(t-\tau) + \frac{1}{2}A^2(t-\tau)^2 + \dots + \frac{1}{k!}A^k(t-\tau)^k + \dots$$



Useful for computing $\Phi(t)$ for small enough $t - \tau$.

The solution is

$$\underline{y}(t) = C\underline{x}(t)$$

$$\underline{x}(t) = e^{A(t-t_0)}\underline{x}(t_0) + \int_{t_0}^t e^{A(t-\tau)} B\underline{u}(\tau) d\tau$$

For $t_0 \rightarrow \infty$:

$$\begin{aligned} \underline{x}(t) &= \int_{-\infty}^t e^{A(t-\tau)} B\underline{u}(\tau) d\tau \\ &= \int_0^{\infty} e^{-A\tau'} B\underline{u}(t-\tau') d\tau' \end{aligned}$$

and for a single input, single output (SISO) system,

$$w(t) = \underline{c}^T e^{At} \underline{b}$$

If $x(t) = e^{j\omega t}$ for all past time

$$\begin{aligned} y(t) &= \int_0^{\infty} w(\tau) e^{j\omega(t-\tau)} d\tau \\ &= \left[\int_0^{\infty} w(\tau) e^{-j\omega\tau} d\tau \right] e^{j\omega t} \\ &= F(\omega)x(t) \end{aligned}$$

Since $w(\tau) = 0$ for $\tau < 0$ for a realizable system, we see that the *steady state sinusoidal response function*, $F(\omega)$, for a system is the Fourier transform of the weighting function - where the coefficient unity must be used.

$$F(\omega) = \int_{-\infty}^{\infty} w(\tau) e^{-j\omega\tau} d\tau$$

and $w(\tau)$ for a stable system is Fourier transformable.

Then

$$w(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

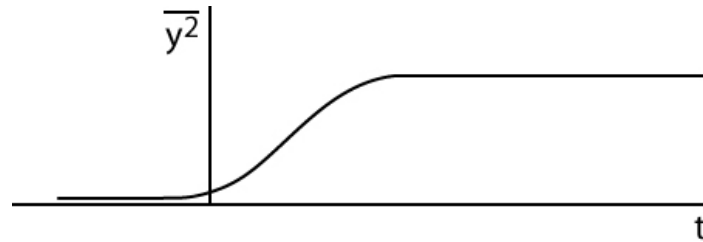
You can compute the response to any input at all, including transient responses, having defined $F(\omega)$ for all frequencies.

The *static sensitivity* of the system is the zero frequency gain, $F(0)$, which is just the integral of the weighting function.

$$F(0) = \int_0^{\infty} w(\tau) d\tau$$

Stationary statistics

Invariant output statistics implies more than stationary inputs and invariant systems; it also implies that the system has been in operation long enough under the present conditions to have exhausted all transients.



Input-Output Relations for Correlation and Spectral Density Functions

Derive autocorrelation of output in terms of autocorrelation of input

$$y(t) = \int_0^{\infty} w(\tau_1)x(t - \tau_1)d\tau_1$$

$$\bar{y} = \int_0^{\infty} w(\tau_1)\bar{x}d\tau_1$$

$$= \bar{x} \int_0^{\infty} w(\tau_1)d\tau_1$$

$$R_{yy}(\tau) = \overline{y(t)y(t + \tau)}$$

$$= \int_0^{\infty} d\tau_1 w(\tau_1) \int_0^{\infty} d\tau_2 w(\tau_2) \overline{x(t - \tau_1)x(t + \tau - \tau_2)}$$

$$= \int_0^{\infty} d\tau_1 w(\tau_1) \int_0^{\infty} d\tau_2 w(\tau_2) R_{xx}(\tau + \tau_1 - \tau_2)$$

$$\overline{y^2} = \int_0^{\infty} d\tau_1 w(\tau_1) \int_0^{\infty} d\tau_2 w(\tau_2) R_{xx}(\tau_1 - \tau_2)$$

$$R_{xy}(\tau) = \overline{x(t)y(t + \tau)}$$

$$= \overline{x(t) \int_0^{\infty} w(\tau_1)x(t + \tau - \tau_1)d\tau_1}$$

$$= \int_0^{\infty} w(\tau_1) R_{xx}(\tau - \tau_1)d\tau_1$$

Transform to get power density spectrum of output.

$$\bar{y} = \bar{x} \int_0^{\infty} w(\tau) d\tau$$

$$= F(0)\bar{x}$$

$$S_{yy}(\omega) = \int_{-\infty}^{\infty} R_{yy}(\tau) e^{-j\omega\tau} d\tau$$

$$= \int_{-\infty}^{\infty} d\tau \int_0^{\infty} d\tau_1 w(\tau_1) \int_0^{\infty} d\tau_2 w(\tau_2) R_{xx}(\tau + \tau_1 - \tau_2) e^{-j\omega\tau}$$

$$= \underbrace{\int_{-\infty}^{\infty} d\tau R_{xx}(\tau + \tau_1 - \tau_2) e^{-j\omega(\tau + \tau_1 - \tau_2)}}_{\text{first integral}} \int_0^{\infty} d\tau_1 w(\tau_1) e^{j\omega\tau_1} \int_0^{\infty} d\tau_2 w(\tau_2) e^{-j\omega\tau_2}$$

In first integral only, let $\begin{cases} \tau' = \tau + \tau_1 - \tau_2 \\ d\tau' = d\tau \end{cases}$

$$S_{yy}(\omega) = \int_{-\infty}^{\infty} d\tau' R_{xx}(\tau') e^{-j\omega\tau'} \int_{-\infty}^{\infty} d\tau_1 w(\tau_1) e^{j\omega\tau_1} \int_{-\infty}^{\infty} d\tau_2 w(\tau_2) e^{-j\omega\tau_2}$$

$$= S_{xx}(\omega) F(-\omega) F(\omega)$$

$$= |F(\omega)|^2 S_{xx}(\omega)$$

The power spectral density thus does not depend upon phase properties.

The *cross-spectral density function* can be derived similarly, to obtain:

$$S_{xy}(\omega) = F(\omega) S_{xx}(\omega)$$

Mean squared output in time and frequency domain

$$\overline{y^2} = R_{yy}(0) = \int_0^{\infty} d\tau_1 w(\tau_1) \int_0^{\infty} d\tau_2 w(\tau_2) R_{xx}(\tau_1 - \tau_2)$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} S_{yy}(\omega) d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) F(-\omega) S_{xx}(\omega) d\omega$$

Generally speaking, with linear invariant systems it is easier to work in the transform domain than the time domain – so we shall commonly use the last expression to calculate the mean squared output of a system. However, control engineers are more accustomed to working with Laplace transforms than with Fourier transforms. By making the change of variables $s = j\omega$ we can cast this expression in that form.

$$\begin{aligned} \overline{y^2} &= \frac{1}{2\pi} \int_{-j\infty}^{j\infty} F\left(\frac{s}{j}\right) F\left(-\frac{s}{j}\right) S_{xx}\left(\frac{s}{j}\right) \frac{ds}{j} \\ &= \frac{1}{2j\pi} \int_{-\infty}^{\infty} F'(s) F'(-s) S'_{xx}(s) ds \end{aligned}$$

We know that $S_{xx}(\omega)$ is even. If it is a rational function of ω , and we will work exclusively with rational spectra, it is then a rational function of ω^2 . So only even powers of ω appear in $S_{xx}(\omega)$ and thus $S_{xx}\left(\frac{s}{j}\right)$ which we may call $S_{xx}(s)$ is derived from $S_{xx}(\omega)$ by replacing ω^2 by $-s^2$.

$F'(s)$ is the ordinary transfer function of the system – the Laplace transform of its weighting function. Because $w(t) = 0, t < 0$.

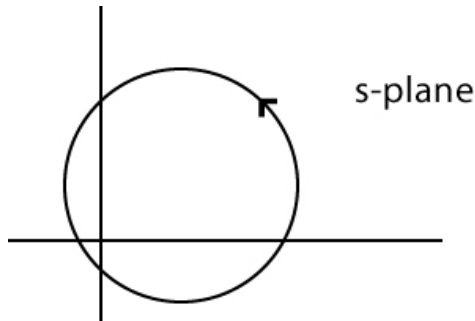
We shall drop the primes from now on.

$$\begin{aligned} \overline{y^2} &= \frac{1}{2\pi j} \int_{-j\infty}^{j\infty} F(s) F(-s) S_{xx}(s) ds \\ &\left. \begin{aligned} \omega^2 &= -s^2 \\ \omega^4 &= s^4 \end{aligned} \right\} \text{in } S_{xx}(s) \end{aligned}$$

Integrating the output spectrum

General method

Cauchy Residue Theorem



$$\oint_C F(s) ds = 2\pi j \sum (\text{residues of } F(s) \text{ at the poles enclosed in the contour } C)$$

If $F(s)$ has a pole of order m at $z = a$,

$$\text{Res}(a) = \frac{1}{(m-1)!} \left\{ \frac{d^{m-1}}{ds^{m-1}} [(s-a)^m F(s)]_{s=a} \right\}$$

$F(s)$ has a pole of order m at $s = a$ if m is the smallest integer for which

$$\lim_{s \rightarrow a} \left[(s - a)^m F(s) \right]$$

is finite.

If $F(s)$ is rational and has a 1st order pole at a ,

$$\begin{aligned} F(s) &= \frac{N(s)}{D(s)} \\ &= \frac{N(s)}{(s - a)(s - b)\dots} \end{aligned}$$

then

$$\begin{aligned} \text{Res}(a)_{m=1} &= \lim_{s \rightarrow a} \left[(s - a)F(s) \right] \\ &= \frac{N(a)}{(a - b)(a - c)\dots} \end{aligned}$$