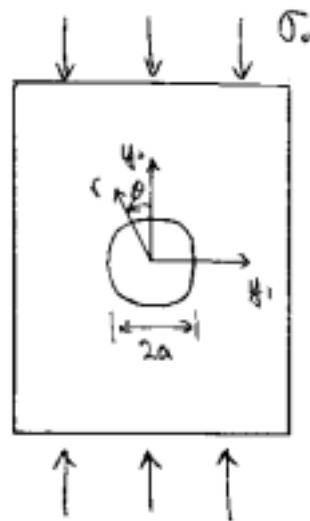


Solutions to Home Assignment #4

Warm-up Exercises

1. To find the expressions for the stress components at the hole boundary as a function of θ , we will use the Airy stress functions. The problem we need to consider is an isotropic plate with a hole under compressive load.



From our notes (unit 8, p.20), our assumed stress function, ϕ , for an isotropic plate with a hole in polar coordinates is

$$\begin{aligned} \phi(r, \theta) = & [A_0 + B_0 \ln r + C_0 r^2 + D_0 r^2 \ln r] \\ & + [A_2 r^2 + \frac{B_2}{r} + C_2 r^4 + D_2] \cos 2\theta \quad \text{--- ①} \end{aligned}$$

In order for the displacements to be single-valued, D_0 is set to equal to zero. For the stresses to be bounded as $r \rightarrow \infty$, C_2 also needs to be zero. The stress in polar coordinates can now be expressed as:

$$\begin{aligned}\sigma_{rr} &= \frac{1}{r} \frac{\partial \phi}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \theta^2} \\ &= \frac{B_0}{r^2} + 2C_0 - \left[2A_2 + \frac{6B_2}{r^2} \right] \cos 2\theta \quad \text{--- ②}\end{aligned}$$

$$\begin{aligned}\sigma_{\theta\theta} &= \frac{\partial^2 \phi}{\partial r^2} \\ &= -\frac{B_0}{r^2} + 2C_0 + \left[2A_2 + \frac{6B_2}{r^2} \right] \cos 2\theta \quad \text{--- ③}\end{aligned}$$

$$\begin{aligned}\sigma_{r\theta} &= -\frac{1}{r} \frac{\partial^2 \phi}{\partial r \partial \theta} + \frac{1}{r^2} \frac{\partial \phi}{\partial \theta} \\ &= \left[2A_2 - \frac{6B_2}{r^2} - \frac{2D_2}{r^2} \right] \sin 2\theta \quad \text{--- ④}\end{aligned}$$

The boundary conditions are:

$$\sigma_{rr} = \sigma_{r\theta} = 0 \quad \text{①} \quad r = a \quad \leftarrow \text{stress-free at hole edge.}$$

$$\sigma_{yy} = \sigma_0, \quad \sigma_{xy} = 0 \quad \text{②} \quad y_2 \rightarrow \infty$$

$$\sigma_{xx} = 0, \quad \sigma_{xy} = 0 \quad \text{③} \quad y_1 \rightarrow \infty$$

Using these boundary conditions, we can find the unknown constants in equations ② through ④. Skipping the math (as described in ^{with p. 26} notes), we can get

$$\sigma_{rr} = \frac{\sigma_c}{2} \left(1 - \frac{a^4}{r^4}\right) + \frac{\sigma_o}{2} \left(1 - 4\frac{a^4}{r^4} + 3\frac{a^6}{r^6}\right) \cos 2\theta \quad \text{--- ⑤}$$

$$\sigma_{\theta\theta} = \frac{\sigma_c}{2} \left(1 + \frac{a^4}{r^4}\right) - \frac{\sigma_o}{2} \left(1 + 3\frac{a^6}{r^6}\right) \cos 2\theta \quad \text{--- ⑥}$$

$$\sigma_{r\theta} = -\frac{\sigma_c}{2} \left(1 + 2\frac{a^4}{r^4} - 3\frac{a^6}{r^6}\right) \sin 2\theta \quad \text{--- ⑦}$$

At the hole boundary, i.e., $r=a$, the stresses are reduced to

$$\sigma_{rr} = 0 \quad \text{--- ⑧}$$

$$\sigma_{\theta\theta} = -\sigma_o (1 - 2 \cos 2\theta) \quad \text{--- ⑨}$$

$$\sigma_{r\theta} = 0 \quad \text{--- ⑩}$$

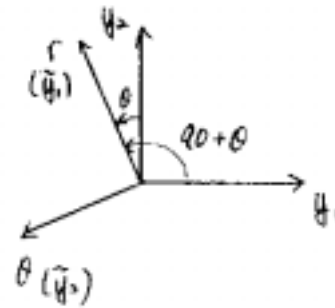
Now, we need to transform our stresses from the polar to Cartesian system.

Set

$$\tilde{\sigma}_{11} = \sigma_{rr} = 0$$

$$\tilde{\sigma}_{22} = \sigma_{\theta\theta}$$

$$\tilde{\sigma}_{12} = \sigma_{r\theta} = 0$$



To transform our r, θ (i.e. \tilde{y}_1, \tilde{y}_2) system to our y_1, y_2 system, we must rotate through an angle $-(90 + \theta)$.

The transformation rule is

$$\sigma_{\alpha\beta} = l_{2\alpha} l_{1\beta} \tilde{\sigma}_{22} \quad \text{--- (1)}$$

This equation reduces to

$$\sigma_{11} = l_{12} l_{12} \tilde{\sigma}_{22} = \cos^2 \theta \sigma_{\theta\theta} \quad \text{--- (2)}$$

$$\sigma_{22} = l_{22} l_{22} \tilde{\sigma}_{22} = \cos^2(90 + \theta) \sigma_{\theta\theta} = \sin^2 \theta \sigma_{\theta\theta} \quad \text{--- (3)}$$

$$\sigma_{12} = l_{12} l_{22} \tilde{\sigma}_{22} = (-\cos \theta)(-\sin \theta) \sigma_{\theta\theta} = \sin \theta \cos \theta \sigma_{\theta\theta} \quad \text{--- (4)}$$

$$\ast \quad l_{12} = \cos(-90 - \theta) = -\sin \theta$$

$$l_{22} = \cos(0 - \theta) = \cos \theta$$

Therefore, plugging the expression for $\sigma_{\theta\theta}$ in equations (12) through (14), we get:

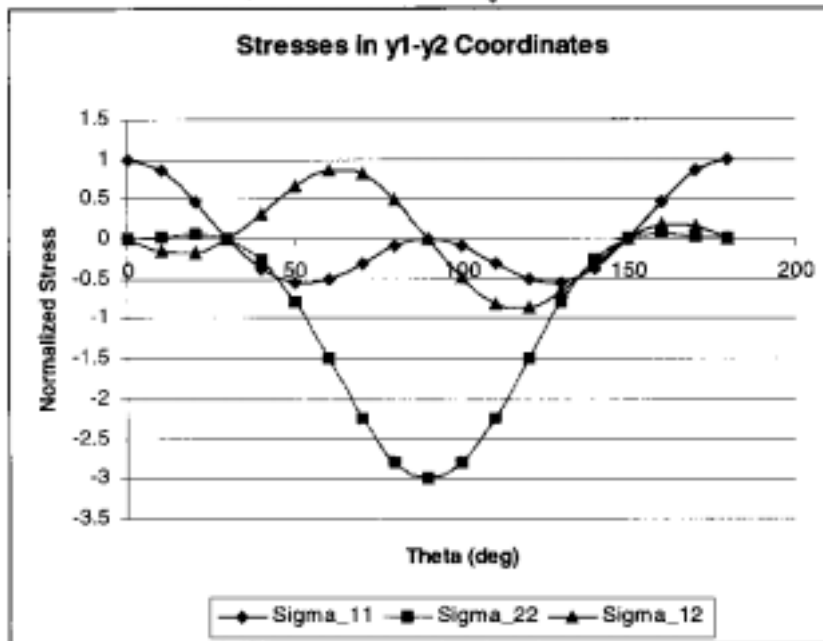
$$\begin{aligned}\sigma_{11} &= -\sigma_0(1-2\cos 2\theta)\cos^2\theta \\ \sigma_{22} &= -\sigma_0(1-2\cos 2\theta)\sin^2\theta \\ \sigma_{12} &= \sigma_0(1-2\cos 2\theta)\sin\theta\cos\theta\end{aligned}$$

For use in problems 2 and 3, the stress can be expressed in normalized form as:

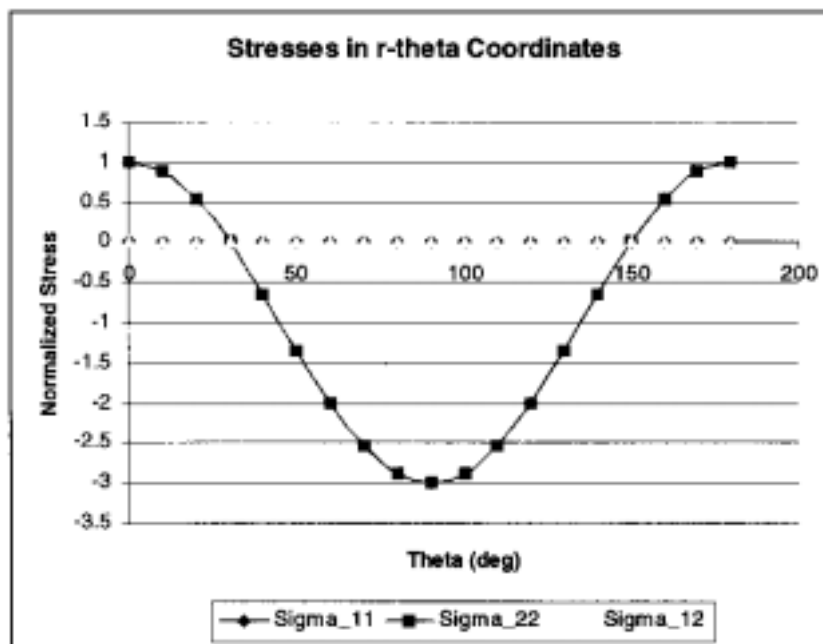
$$\begin{aligned}\text{y}_1\text{-y}_2 \text{ coordinate:} \quad \sigma_{11}/\sigma_0 &= -(1-2\cos 2\theta)\cos^2\theta \\ \sigma_{22}/\sigma_0 &= -(1-2\cos 2\theta)\sin^2\theta \\ \sigma_{12}/\sigma_0 &= (1-2\cos 2\theta)\sin\theta\cos\theta\end{aligned}$$

$$\begin{aligned}\text{r-}\theta \text{ coordinate:} \quad \sigma_{rr}/\sigma_0 &= 0 \\ \sigma_{\theta\theta}/\sigma_0 &= -(1-2\cos 2\theta) \\ \sigma_{r\theta}/\sigma_0 &= 0\end{aligned}$$

2. Stresses in y_1 - y_2 coordinate system



3. Stresses in r - θ coordinate system



4. We can derive a number of interesting results from these plots.

- ① Extensional stresses (σ_{rr} , $\sigma_{\theta\theta}$, $\sigma_{\phi\phi}$) are symmetric about each 90° rotation.
- ② Shear stresses ($\sigma_{r\theta}$) are anti-symmetric about each 90° rotation.
- ③ All stresses go to zero at $\theta = 30^\circ, 150^\circ, 210^\circ$ and 330° .
- ④ σ_{rr} and $\sigma_{r\theta}$ are zero at hole edge. Only $\sigma_{\theta\theta}$ is non-zero.
- ⑤ In the plots, all stresses are normalized by σ_0 , which is negative in the present case. So, the actual stress state has the same shape but opposite sign.